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in Agricultural Dryers*

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Project Director: *Dr. J. H. Schlag*

Sponsor: *U. S. Department of Agriculture; Science and Education Administration
Agricultural Research - Southern Region; New Orleans, LA 70153*

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QUARTERLY REPORT

Submitted to the
Department of Energy
Through the U.S. Department of Agriculture

from

Georgia Institute of Technology
225 North Avenue, N.W.
Atlanta, Georgia 30332

CONTROL SYSTEMS FOR INTERFACING SOLAR AND
BIOMASS FUELS IN AGRICULTURAL DRYERS

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INTRODUCTION

Previous work has shown that solar energy is a feasible alternative to fossil fuels for crop drying. However, the greatest drawback to solar energy is that it is not continuously available, and other energy sources must be used as backup. Research is being conducted into the use of biomass to generate methane and alcohol which could be used as backup fuels for solar dryers. It is the objective of this paper to examine the interfacing problem between a solar dryer and a biomass-fueled backup system.

The equipment setup is shown in Figure 1. The valves to ambient air and the solar collectors will be controlled by a microprocessor, as will the amount of biomass gas inlet. The inputs to the microprocessor will include ambient humidity, ambient air temperature, solar collector temperature, intermediate air temperature, the state of the blower fan (on or off), the drying temperature of the air, and the humidity of the drying chamber; the outputs will be the controls on the valve openings and gas inlet. The model which has been developed is essentially a static description of the relationships involved. However, because of the large time-span involved in drying crops (of the order of 24 hours) and the slow response time of valve mechanisms, static relationships can be employed by the microprocessor in an iterative manner, effectively producing a slow-dynamic model.

The first question addressed by the model is how the ideal drying temperature for a particular substance determines the length of time required to bring the moisture content from some initial level to a pre-

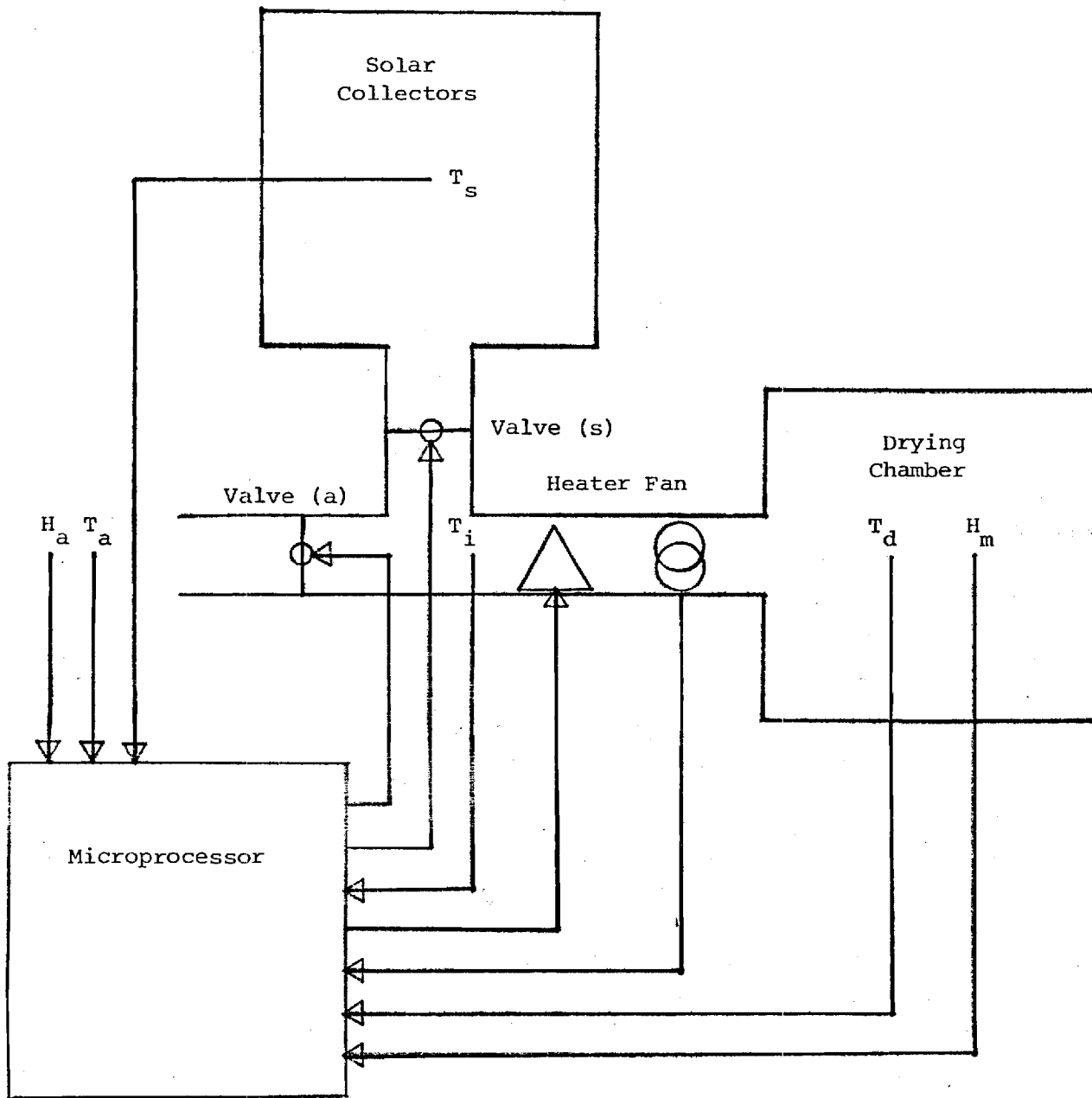


FIGURE 1

determined final level.

The second question addressed is what combination of ambient air, solar-heated air, and additional biomass thermal power is most appropriate and economical under prevailing climatic conditions, i.e., ambient temperature, insolation, etc.

Finally the desired rates of flow of ambient air and solar-heated air must be related to the angular openings of the two valves and to any resistance to air flow (drag) inherent in the two sources.

DEFINITION OF SYMBOLS

Let symbols be defined as follows:

Q_{req} = heat energy required for drying

Q_{sup} = heat energy supplied by ambient air, solar collectors, biomass
fuel, or some combination of these three

m = mass of matter to be dried

M = mass of air used in drying

μ_i = initial water fraction in matter to be dried

μ_f = final water fraction in matter to be dried

c_w = specific heat capacity of water = 1.0 Kcal/KgC°

c_a = specific heat capacity of ambient air

h_v = heat of vaporization of water

h_c = heat of combustion of biomass fuel (alcohol or methane)

T_a = temperature (°C) of ambient air

T_s = temperature of solar collector system

T_d = ideal drying temperature for a particular type of matter

T_m = initial temperature of matter to be dried

T_i = temperature of warm air before heating by biomass fuel

H_a = ambient humidity

ρ_a = density of ambient air

H_m = humidity of drying chamber

\dot{V}_d = total volume flow rate provided by fan, assumed constant

\dot{V}_a = volume flow rate of ambient air

\dot{V}_s = volume flow rate of solar-heated air

Δt = time duration of drying process

\dot{q}_{req} = thermal power required from biomass fuel

\dot{q}_{sup} = thermal power supplied by biomass fuel

\dot{v} = volume flow rate for gas (alcohol or methane) in the biomass heater

θ = angle of opening of valve to ambient air

ϕ = angle of opening of valve to solar collector system

r = radius of duct pipe

EXPLANATION OF MODEL

I. From a consideration of the expressions for Q_{req} and Q_{sup} the relation between T_d and Δt can be shown:

$$Q_{\text{req}} = (\mu_i - \mu_f)m c_w(T_d - T_m) + (\mu_i - \mu_f)m h_v(H_m, T_d) \quad (1)$$

Note that vaporization occurs at $T_d < 100^\circ\text{C}$, and that the heat of vaporization will be a function of both humidity and temperature.

$$\begin{aligned} Q_{\text{sup}} &= M c_a(H_a)T_d \\ &= \rho_a \dot{V}_d \Delta t c_a(H_a)T_d \end{aligned} \quad (2)$$

Here note that the specific heat of air will be a function of humidity.

By recognizing that Q_{sup} must equal Q_{req} , and that ρ_a , \dot{V}_d , and $c_a(H_a)$ are not adjustable, it follows that T_d determines Δt .

II. The discussion now concerns how usage of ambient air, solar-heated air and biomass fuel is determined.

- A. If $T_a = T_d$, then open only the valve to ambient air, leaving valve to solar system closed and biomass heater off. In this case $\dot{V}_a = \dot{V}_d$, and $\dot{V}_s = 0$.
- B. If $T_a < T_d$ and $T_s = T_d$, then open only the valve to the solar system, leaving valve to ambient air closed and biomass heater off. In this case $\dot{V}_s = \dot{V}_d$, and $\dot{V}_a = 0$.
- C. If $T_a < T_d$ and $T_s > T_d$, then leave biomass heater off and open both valves (to ambient air and solar system) to appropriate

degrees so that

$$\begin{cases} \dot{V}_a + \dot{V}_s = \dot{V}_d \\ T_a \dot{V}_a + T_s \dot{V}_s = T_d \dot{V}_d \end{cases} \quad (3)$$

whose solution is

$$\begin{aligned} \dot{V}_a &= \dot{V}_d \left(\frac{T_s - T_d}{T_s - T_a} \right) \\ \dot{V}_s &= \dot{V}_d \left(\frac{T_d - T_a}{T_s - T_a} \right) \end{aligned} \quad (4)$$

D. Finally, if $T_a < T_d$ and $T_s < T_d$, then extra heat energy will have to be added by the biomass-powered heater.

In this case

$$\begin{aligned} \dot{V}_a + \dot{V}_s &= \dot{V}_d \\ T_a \dot{V}_a + T_s \dot{V}_s &= T_i \dot{V}_d < T_d \dot{V}_d \end{aligned} \quad (5)$$

$$\text{and } T_i < T_d$$

In order to raise T_i to T_d , \dot{q}_{req} Kcal/sec must be added, where

$$\begin{aligned} \dot{q}_{\text{req}} &= \frac{d}{dt} \left[M c_a (H_a) (T_d - T_i) \right] \\ &= c_a (H_a) (T_d - T_i) \rho_a \dot{V}_d \end{aligned} \quad (6)$$

The thermal power supplied is given by

$$\dot{q}_{\text{sup}} = h_c \dot{v} \quad (7)$$

Since \dot{q}_{sup} must equal \dot{q}_{req} , T_i determines \dot{v} .

- E. Although there will be a thermocouple positioned to measure the temperature T_i of the air mixed from the ambient air valve and the solar system valve, it is a simple matter to calculate it from T_a , \dot{v}_a , T_s , and \dot{v}_s .

$$T_i = \frac{T_a \dot{v}_a + T_s \dot{v}_s}{\dot{v}_a + \dot{v}_s} \quad (8)$$

Even though it is intuitively apparent in this form as a weighted average, the expression can also be found by using a simple heat transfer calculation.

- III. It remains to discuss how the volume flow rate for a valve depends on angular opening and on any resistive structures within. When the two valves are used together, these flow rates will be coupled, as stated earlier.

$$\dot{v}_a + \dot{v}_s = \dot{v}_d$$

It will be useful to consider an analogous electrical circuit. Let the resistance within the ambient air system be R_a , that within the solar system be R_s . Let the resistance offered by the ambient air valve (open to angle θ) be R_θ , that offered by the solar system valve (open to angle ϕ) be R_ϕ . Let the total air flow rate \dot{v}_d be represented by the total current in the circuit i_d , and the flow rates in the "parallel" valves by i_a and i_s . The source of emf

(pressure) is E. A diagram of the circuit is given in Figure 2.

The solutions to this circuit for $i_a(\dot{V}_a)$ and $i_s(\dot{V}_s)$ are given by:

$$i_a = i_d \left(\frac{R_s + R_\phi}{R_a + R_\theta + R_s + R_\phi} \right) \quad (9)$$

$$i_s = i_d \left(\frac{R_a + R_\theta}{R_a + R_\theta + R_s + R_\phi} \right)$$

It is clear from the solutions to this analogous electrical circuit that the drag factors in the two air paths of the drying system will be closely coupled. Since there is no a priori way of modeling the air drag quantities represented by R_a , R_θ , R_s , and R_ϕ , empirical measurements will be used to obtain their relative magnitudes. One useful relationship can be obtained, however. It seems reasonable that the amount of drag presented to the air flow by a valve will be proportional to the projected area of the valve on the plane of the opening; thus

$$R_\theta \propto \pi r^2 \cos \theta \text{ and } R_\phi \propto \pi r^2 \cos \phi \quad (10)$$

Where it is assumed that the radius of the duct pipe r will be the same throughout the system. Nevertheless, an exact understanding of the magnitudes of these four drag factors will not be necessary because of the iterative control procedure employed: an initial setting of the air valves and gas inlet will be determined by the input parameters; the intermediate temperature and ultimate drying temperature will be checked; the air valves and gas inlet will be re-set, if necessary; then temperatures will be re-checked and the iteration process continued.

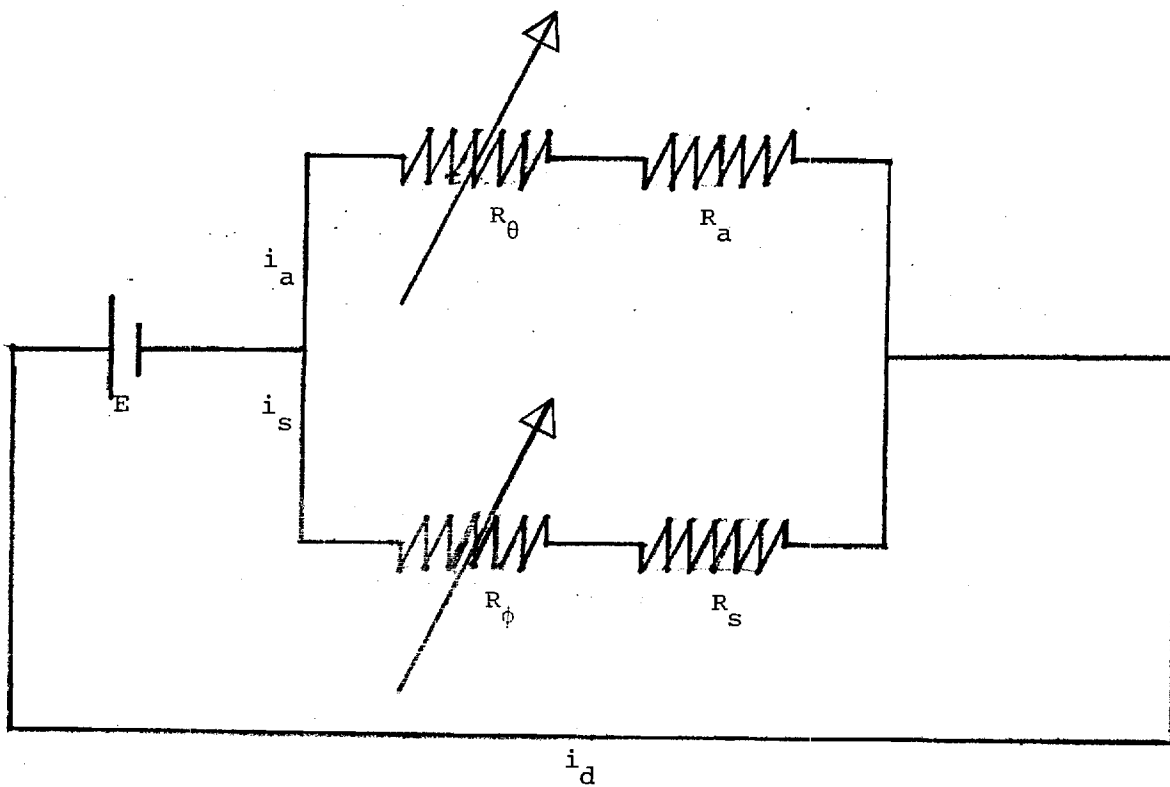


FIGURE 2

CONCLUSION

The discussion has treated the component parts of this interfacing problem by simple modeling procedures. Although the mathematical relationships could be further explored in various places, it is felt that the iterative nature of the control process will be adequate to refine the approximations made by the model.

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January 1980

INTRODUCTION

The previous quarterly report included a description of a theoretical model for mixing solar heated air, ambient air, and heat from an auxiliary source such as a biomass convertor. Functional equations were provided to describe the physics involved in the operation of the system. The model represents a means for establishing an ideal environment for drying crops, as well as optimizing the use of solar and thermal power under variable climatic conditions.

EXPERIMENTAL MODEL

In order to test the theory put forth in the report of last October, an experimental model has been designed and is under construction. A functional diagram of the equipment involved is presented in Figure 1, which uses the same symbology as the earlier report. Most of the symbol definitions are given again in the next section.

The ductwork for the model is made of galvanized aluminum "stove pipe." Thermocouple temperature probes and air flow meters are positioned as shown. The air from the chamber representing the solar collectors will be heated by an alternate source so that the entire unit can be assembled and operated within the laboratory. This is necessary since the lab contains the facilities which are essential for developing the microprocessor software.

This software will contain the algorithm to calculate the desired setting for the dampers based on the ambient temperature, the temperature of the air from the solar collector (representing climatic condi-

tions), and the selected range for the dryer temperature. The equations presented in the previous report are incorporated in the algorithm.

The valves shown in Figure 1 are actually dampers that are 90 degrees out-of-phase; that is, when one is completely open permitting maximum air flow, the other is closed for minimum air flow through the pipe. The two dampers are physically linked so that as one damper is closing the other is opening. The stepping motor, which provides the power to operate the dampers, receives signals from the microprocessor indicating whether the motor should rotate clockwise or counterclockwise and by how many increments.

SOFTWARE

A flowchart of the microprocessor's control program is shown in Appendix A. The symbols are defined as:

- H_M - initial humidity of the material to be dried
- T_S - temperature of the "solar" heated air
- H_A - ambient humidity
- T_A - temperature of the ambient air
- T_D - temperature of the drying chamber
- θ - angle of the damper in the solar duct (0° is minimum air flow)
- l - lower limit of dryer temperature range
- u - upper limit of dryer temperature range
- a - program variable for iteratively calculating θ
- α - intermediate angle in calculating proper θ .

When the program is entered initially, the temperature is measured. If the temperature of the solar heated air is within the desired

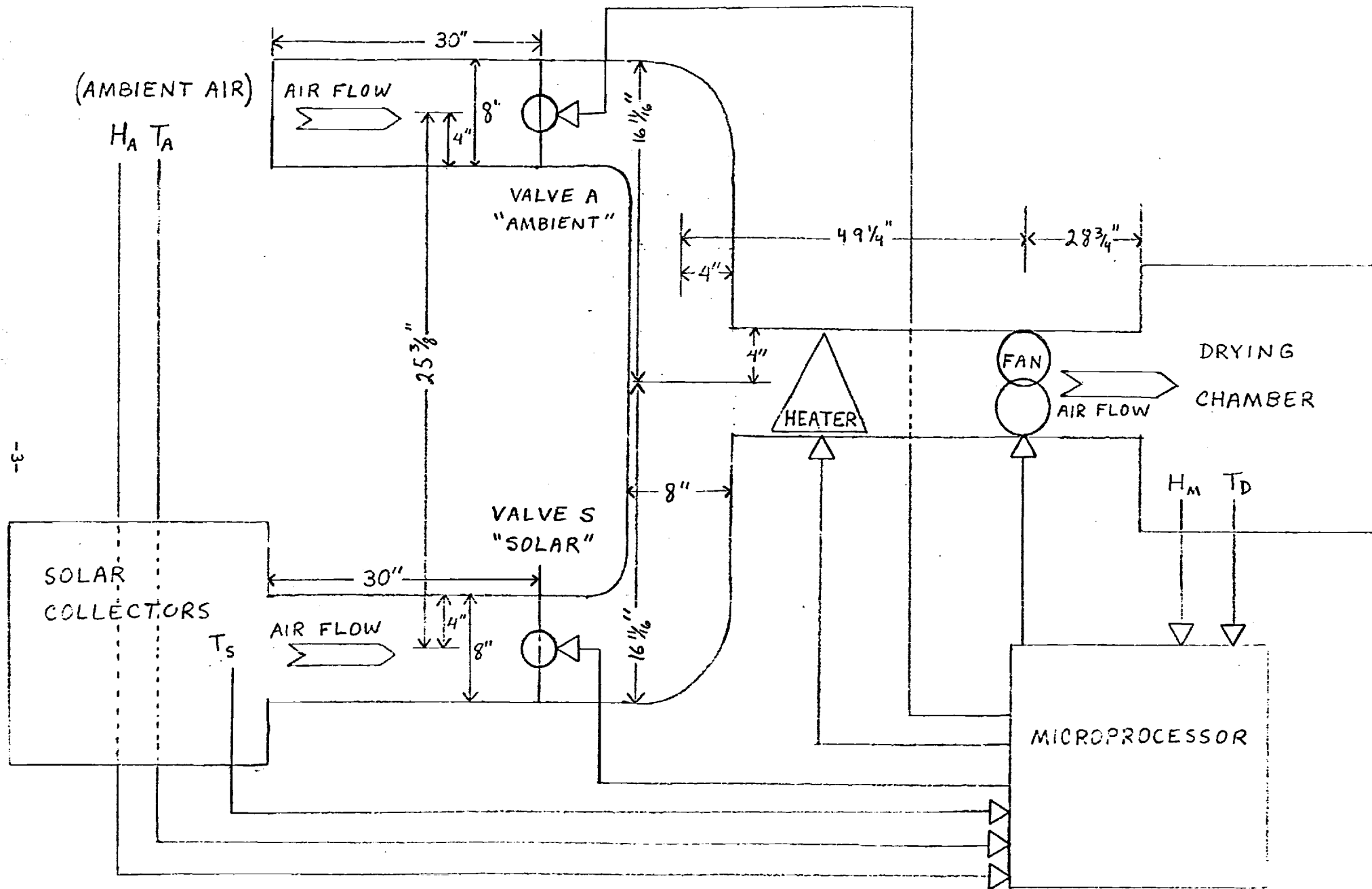


Figure 1. Experimental Model (not to scale)

range for the drying chamber, then the proper dryer temperature T_D can theoretically be attained by using solar heated air alone without intermixing any ambient air. Program operation will remain in this loop (labeled "Max Solar" in the flowchart) until T_S deviates outside the desired range.

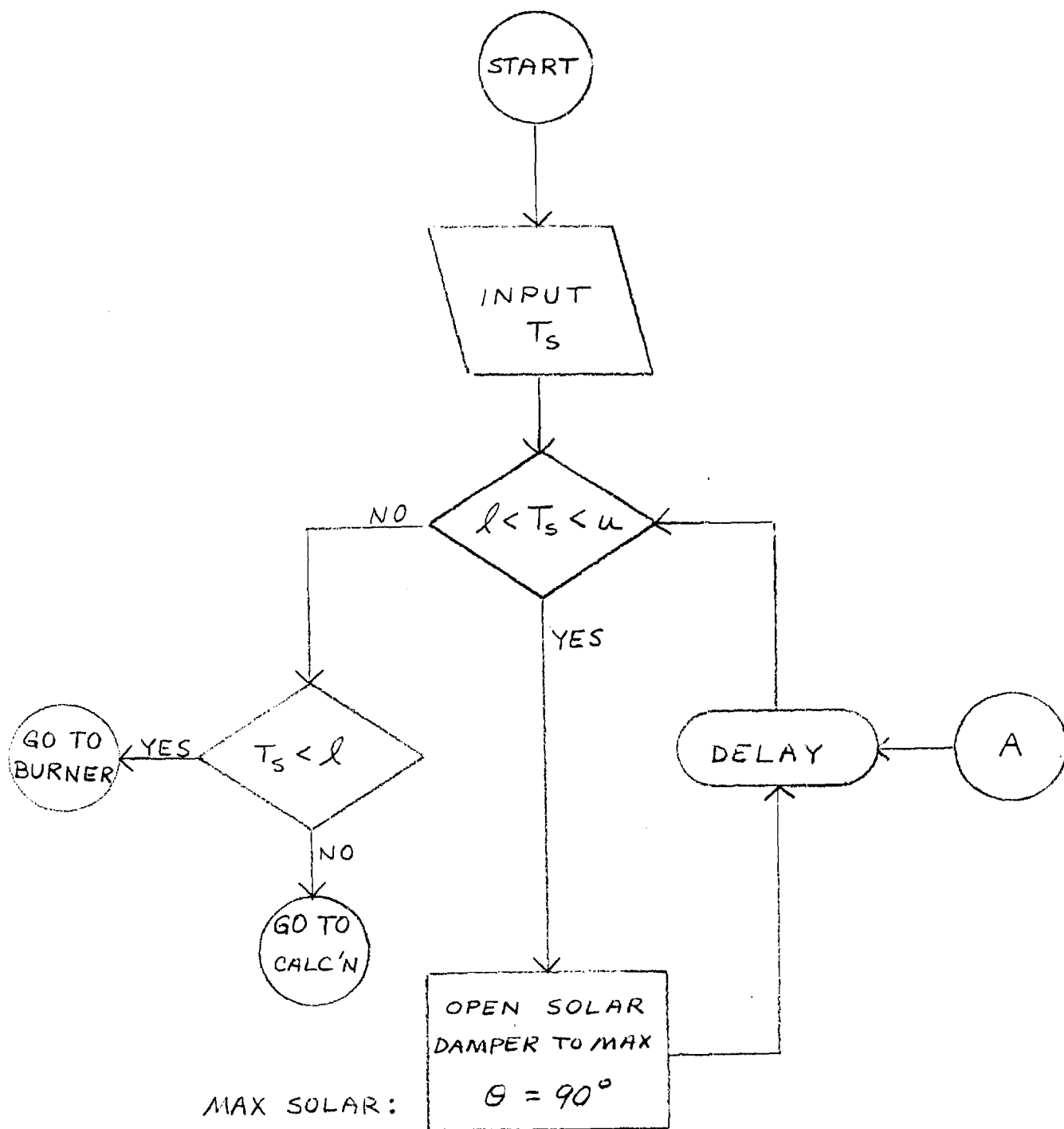
If T_S is found to be below the lower limit, the program will go to the "burner" loop. It is assumed that the ambient air will always be colder than the solar air. If T_S is too low, then the burner must be turned on and left on until the dryer temperature is well within the selected range. Both T_S and T_D are checked within the execution of this loop. If T_S should increase, the program will exit the loop; otherwise, if T_D falls below the lower limit the burner will be turned on again.

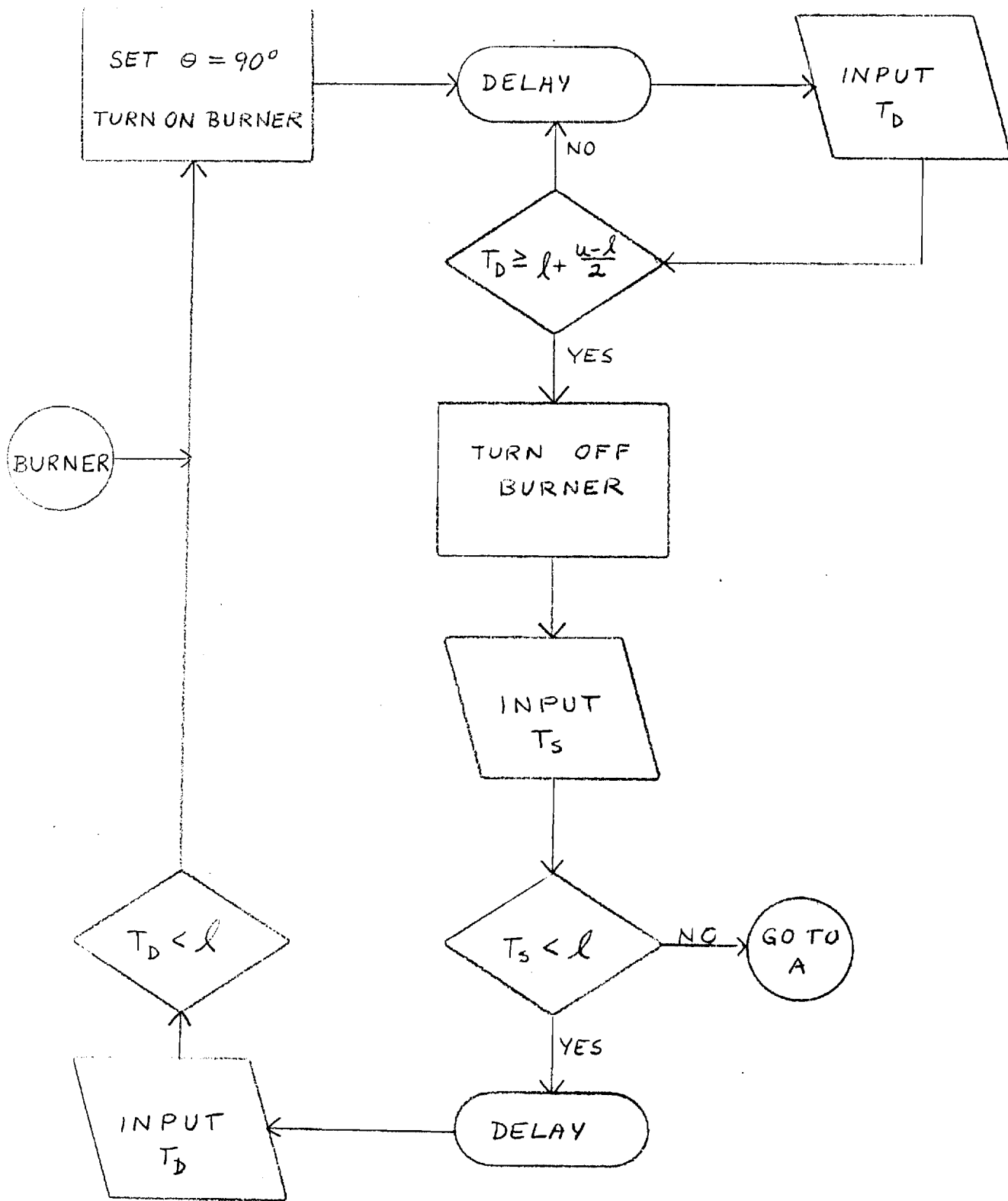
For the case where T_S is above the upper limit, the program will enter the "calculation" loop, which determines the proper value for theta based on the measured temperatures of T_A and T_S . This procedure uses the equations of the October report to select the angular setting for the dampers. According to the theory, after the dampers have been adjusted the dryer temperature should stabilize within the acceptable range. However, if the dryer temperature does not reach an acceptable level after a certain time lapse, the microprocessor will signal the stepping motor to alter theta accordingly. After each incremental adjustment and a time delay, the dryer temperature will be measured again. This routine will continue until T_D falls within the desired limits, after which the temperature T_D is monitored for any further variations.

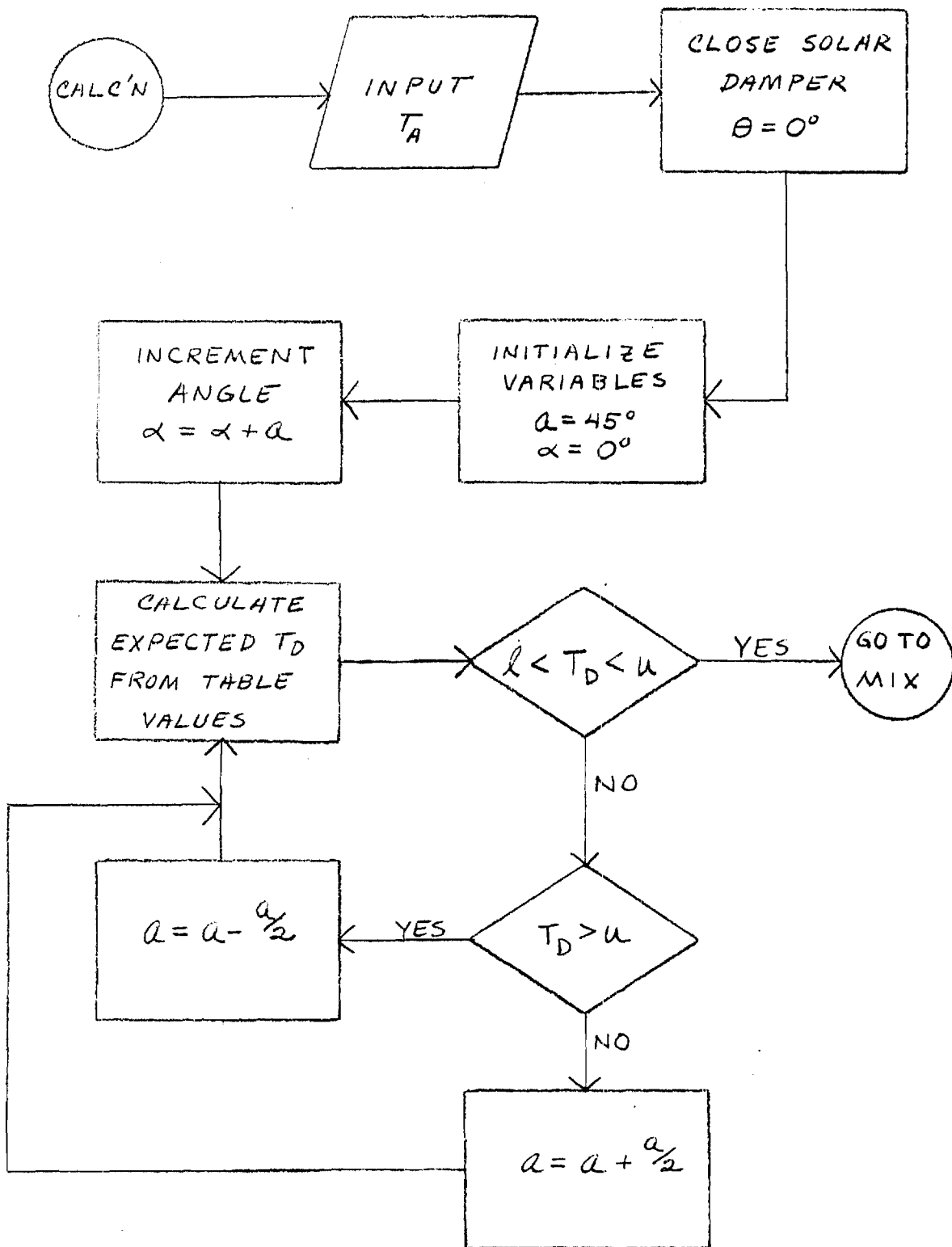
A trial program has been written in PL/M and assembled on an Intel MDS-II development system. Appendix B contains an entire program listing with the assembly code for each PL/M statement. During system testing, this program will be stored in the read-only memory of an SBC (single board computer) model 8020. It can be changed at any time to accommodate modifications to the algorithm, control signals, or program loops.

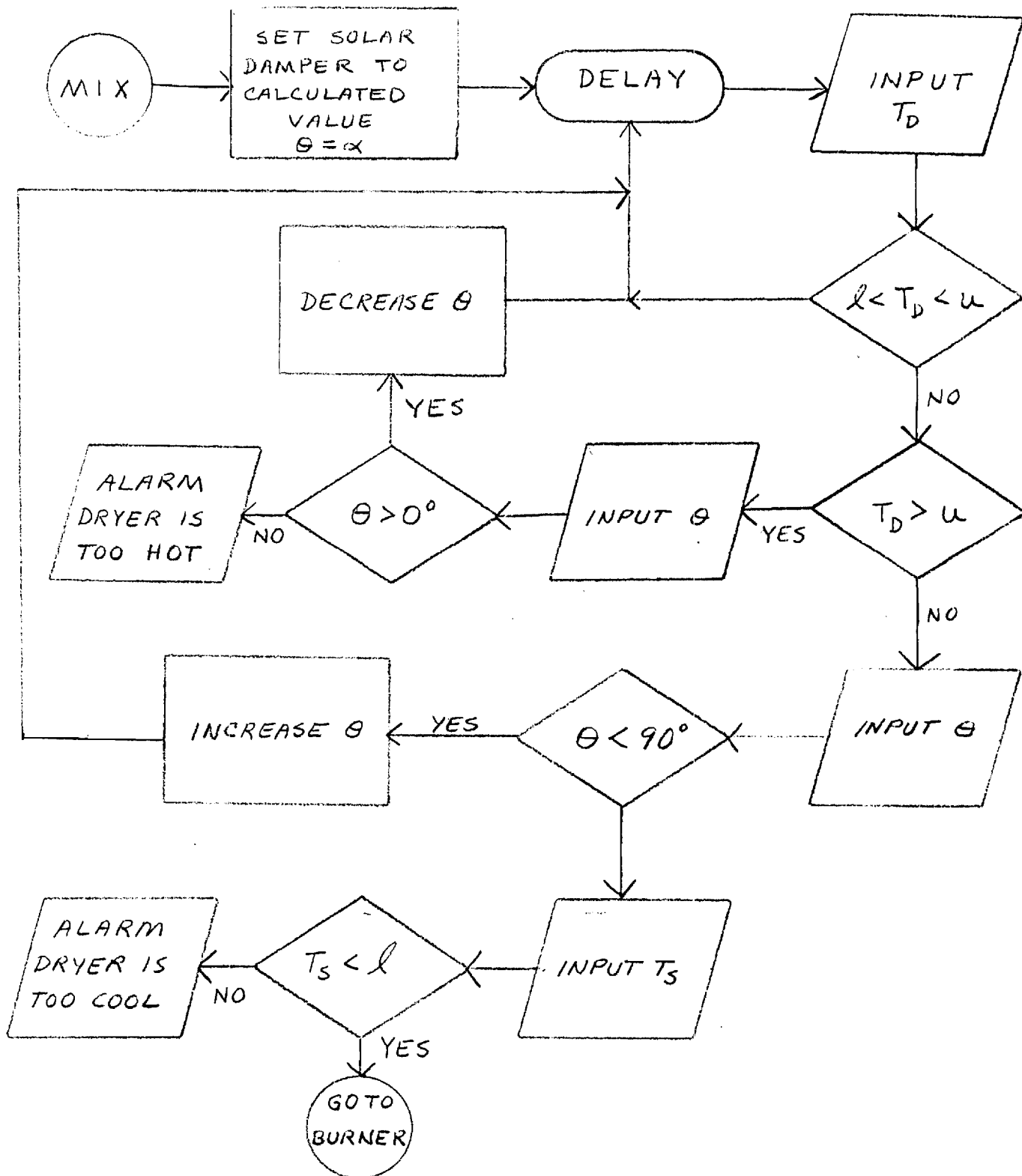
APPENDIX A

Flowchart for Controlling
Dampers and Burners









APPENDIX B

Program Listing for Process Control

ISIS-II PL/M-80 V3.0 COMPILATION OF MODULE USDA

OBJECT MODULE PLACED IN :F1:USDA.OBJ

COMPILER INVOKED BY: PLM80 :F1:USDA.SRC CODE

```

1      USDA:DO;
2  1      DECLARE (TS,TA,TD) ADDRESS;
3  1      DECLARE (ALT,L,J,I,U,A,THETA,N) BYTE INITIAL(1,70,0,0,80,0,0,
4  1      DECLARE KS(50) ADDRESS DATA(3282,1689,1157,891,731,624,547,48
          408,378,353,331,313,296,282,269,258,247,238,229,221,
          213,206,200,194,188,183,178,173,168,163,159,155,151,147,
          143,140,136,132,129,126,122,119,116,113,109,106,103,100);
5  1      DECLARE KA(50) ADDRESS DATA(100,103,106,109,113,116,119,122,1
          132,136,140,143,147,151,155,159,163,168,173,178,183,188,1
          200,206,213,221,229,238,247,258,269,282,296,313,331,353,3
          408,444,489,547,634,731,892,1157,1689,3282);

6  1      FWD:PROCEDURE;
                                     ; STATEMENT # 6
          ; PROC FWD
7  2      OUTPUT(0)=1;
                                     ; STATEMENT # 7
          0354 3E01      MVI      A,1H
          0356 D300      OUT      0H
8  2      CALL TIME(100);
          /*10MS DELAY*/
                                     ; STATEMENT # 8
          0358 3E64      MVI      A,64H
          035A CD0000     CALL     GP0105
9  2      OUTPUT(0)=0;
                                     ; STATEMENT # 9
          035D 3E00      MVI      A,0H
          035F D300      OUT      0H
10 2      CALL TIME(100);
          /*PULSES @ 50HZ*/
                                     ; STATEMENT # 10
          0361 3E64      MVI      A,64H
          0363 CD0000     CALL     GP0105
11 2      END FWD;
                                     ; STATEMENT # 11
          0366 C9      RET
12 1      DELAY:PROCEDURE;
                                     ; STATEMENT # 12
          ; PROC DELAY
13 2      DO I=1 TO 4;
                                     ; STATEMENT # 13
          0367 210900     LXI      H,I
          036A 3601      MVI      M,1H
          Q21:
          036C 3E04      MVI      A,4H
          036E 210900     LXI      H,I
          0371 BE      CMP      M
          0372 DA9603     JC      Q22
14 3      DO J=1 TO 250;
          /*10 SEC DELAY*/
                                     ; STATEMENT # 14
          0375 210800     LXI      H,J
          0378 3601      MVI      M,1H

```

```

                                Q23:
                                MVI    A,0FAH
                                LXI    H,J
                                CMP    M
                                JC      Q24
15   4      CALL TIME(100);
                                ; STATEMENT # 15
                                MVI    A,64H
                                CALL    QP0105
16   4      END;
                                ; STATEMENT # 16
                                LXI    H,J
                                INR     M
                                JNZ     Q23
                                Q24:
17   3      END;
                                ; STATEMENT # 17
                                LXI    H,I
                                INR     M
                                JNZ     Q21
                                Q22:
18   2      END DELAY;
                                ; STATEMENT # 18
                                RET
                                ; STATEMENT # 19
19   1      DEG90:PROCEDURE;
                                ; PROC DEG90
20   2      DO WHILE(SHR((NOT INPUT(0)),1));
                                ; STATEMENT # 20
                                Q25:
                                IN      0H
                                CMA
                                ORA     A
                                RAR
                                RAB
                                JNC      Q26
21   3      CALL FWD;
                                ; STATEMENT # 21
                                CALL    FWD
22   3      END;
                                ; STATEMENT # 22
                                JMP      Q25
                                Q26:
23   2      END DEG90;
                                ; STATEMENT # 23
                                RET
                                ; STATEMENT # 24
24   1      BKWD:PROCEDURE;
                                ; PROC BKWD
25   2      OUTPUT(0)=2; /*RAISE CONTROL LINE FOR BKWD PULSES*/
                                ; STATEMENT # 25
                                MVI    A,2H
                                OUT     0H
26   2      CALL TIME(100); /*10 MS DELAY*/
                                ; STATEMENT # 26

```

```

27  2  03AB 3E64      MVI    A,64H
      03AD CD0000    CALL   @P0105
      OUTPUT(0)=0; /*LOWER CONTROL LINE*/
                        ; STATEMENT # 27

      03B0 3E00      MVI    A,0H
      03B2 D300      OUT     0H
28  2          CALL TIME(100);
                        ; STATEMENT # 28

      03B4 3E64      MVI    A,64H
      03B6 CD0000    CALL   @P0105
29  2          END BKWD;
                        ; STATEMENT # 29

      03B9 C9        RET

30  1          CO:PROCEDURE(CHAR) EXTERNAL;
31  2          DECLARE CHAR BYTE;
32  2          END CO;

33  1          START:DO WHILE (NOT INPUT(0)); /*BIT 0 INDICATES 0 DEGREES*/
                        ; STATEMENT # 33
      00C8 310000    LXI     SP,@STACK$ORIGIN
                        START:
                        @27:
      00CB DB00      IN      0H
      00CD 1F        RAR
      00CE DAD700    JC      @28
34  2          CALL BKWD;
                        ; STATEMENT # 34

      00D1 CDA703    CALL   BKWD
35  2          END;
                        ; STATEMENT # 35

      00D4 C3CB00    JMP     @27
                        @28:

36  1          SOLAR: TS=INPUT(1); /*MEASURE TEMP OF SOLAR HEATED AIR*/
                        ; STATEMENT # 36

                        SOLAR:
      00D7 DB01      IN      1H
      00D9 6F        MOV     L,A
      00DA 2600      MVI     H,0
      00DC 220000    SHLD    TS
37  1          IF(TS>U)THEN GOTO MIX;
                        ; STATEMENT # 37

      00DF 3A0A00    LDA     U
      00E2 CD0000    CALL   @P0094
      00E5 D2EB00    JNC     @1
                        ; STATEMENT # 38

      00E8 C35201    JMP     MIX
                        @1:

39  1          CALL DEG90;
                        ; STATEMENT # 39

      00EB CD9703    CALL   DEG90
40  1          IF(TS<L)THEN GOTO BURNER;
                        ; STATEMENT # 40

      00EE 3A0700    LDA     L
      00F1 110000    LXI     D,TS

```

```

00F4 CD0000          CALL    QP0101
00F7 D2FD00          JNC     Q2
                                ; STATEMENT # 41
00FA C30301          JMP     BURNER
42  1                Q2:
                        ELSE CALL DELAY;
                                ; STATEMENT # 42
00FD CD6703          CALL    DELAY
43  1                Q3:
                        GOTO SOLAR;
                                ; STATEMENT # 43
0100 C3D700          JMP     SOLAR
44  1                BURNER: OUTPUT(0)=4; /*RAISE CONTROL LINE TO LIGHT BURNER*
                                ; STATEMENT # 44
                        BURNER:
0103 3E04          MVI     A,4H
0105 D300          OUT     0H
45  1                DO WHILE(INPUT(3)<L+(U-L)/2); /*INPUT(3) IS TD*/
                                ; STATEMENT # 45
                        Q29:
0107 DB03          IN      3H
0109 210700        LXI     H,L
010C F5            PUSH    PSW ; 1
010D 3A0A00        LDA     U
0110 96            SUB     M
0111 5F            MOV     E,A
0112 1600          MVI     D,0
0114 210200        LXI     H,2H
0117 CD0000        CALL    QP0029
011A 2A0700        LHLD    L
011D 2600          MVI     H,0
011F 19            DAD     D
0120 F1            POP     PSW ; 1
0121 CD0000        CALL    QP0094
0124 D22D01        JNC     Q30
46  2                CALL DELAY;
                                ; STATEMENT # 46
0127 CD6703          CALL    DELAY
47  2                END;
                                ; STATEMENT # 47
012A C30701          JMP     Q29
48  1                Q30:
                        OUTPUT(0)=0; /*TURN OFF BURNER*/
                                ; STATEMENT # 48
012D 3E00          MVI     A,0H
012F D300          OUT     0H
49  1                LOOP: IF (INPUT(1)<L) THEN CALL DELAY; /*IF TS<L*/
                                ; STATEMENT # 49
                        LOOP:
0131 DB01          IN      1H
0133 210700        LXI     H,L
0136 BE            CMP     M
0137 D24001        JNC     Q4
                                ; STATEMENT # 50
013A CD6703          CALL    DELAY

```

```

013D C34301      JMP      Q5
51  1      Q4:      ELSE GOTO SOLAR;      /*IF TS>L*/
                                ; STATEMENT # 51
0140 C3D700      JMP      SOLAR
52  1      Q5:      IF(INPUT(3)<L)THEN GOTO BURNER; /*IF TD<L & TS<L*/
                                ; STATEMENT # 52
0143 DB03        IN        3H
0145 210700      LXI       H,L
0148 BE          CMP       M
0149 D24F01      JNC       Q6
                                ; STATEMENT # 53
014C C30301      JMP      BURNER
54  1      Q6:      ELSE GOTO LOOP; /*IF TD>L & TS<L*/
                                ; STATEMENT # 54
014F C33101      JMP      LOOP
55  1      Q7:
MIX:      TA=INPUT(2);
                                ; STATEMENT # 55
MIX:
0152 DB02        IN        2H
0154 6F          MOV       L,A
0155 2600        MVI       H,0
0157 220200      SHLD      TA
56  1      IF((INPUT(0) AND 1)=1)THEN THETA=0;
                                ; STATEMENT # 56
015A DB00        IN        0H
015C E601        ANI       1H
015E FE01        CPI       1H
0160 C26801      JNZ       Q8
                                ; STATEMENT # 57
0163 210C00      LXI       H,THETA
0166 3600        MVI       M,0H
58  1      Q8:      IF((INPUT(0) AND 2)=2)THEN THETA=50;
                                ; STATEMENT # 58
0168 DB00        IN        0H
016A E602        ANI       2H
016C FE02        CPI       2H
016E C27601      JNZ       Q9
                                ; STATEMENT # 59
0171 210C00      LXI       H,THETA
0174 3632        MVI       M,32H
60  1      Q9:      /*ITERATIVE PROCEDURE FOR DETERMINING THEORETICAL SETTING
N,A=25;
                                ; STATEMENT # 60
0176 210D00      LXI       H,N
0179 3619        MVI       M,19H
017B 210B00      LXI       H,A
017E 3619        MVI       M,19H
61  1      ALT=1;
                                ; STATEMENT # 61

```

```

0180 210600      LXI      H,ALT
0183 3601      MVI      M,1H
62  1      ITER:      TD=TS*100/KS(N)+TA*100/KA(N);
                                ; STATEMENT # 62
                                ITER:
0185 116400      LXI      D,64H
0188 2A0000      LHL D    TS
018B CD0000      CALL     GP0034
018E E5          PUSH     H          ; 1
018F 2A0D00      LHL D    N
0192 2600      MVI      H,0
0194 010000      LXI      B,KS
0197 29          DAD      H
0198 09          DAD      B
0199 4E          MOV      C,M
019A 23          INX      H
019B 46          MOV      B,M
019C D1          POP      D          ; 1
019D CD0000      CALL     GP0030
01A0 D5          PUSH     D          ; 1
01A1 116400      LXI      D,64H
01A4 2A0200      LHL D    TA
01A7 CD0000      CALL     GP0034
01AA E5          PUSH     H          ; 2
01AB 2A0D00      LHL D    N
01AE 2600      MVI      H,0
01B0 016400      LXI      B,KA
01B3 29          DAD      H
01B4 09          DAD      B
01B5 4E          MOV      C,M
01B6 23          INX      H
01B7 46          MOV      B,M
01B8 D1          POP      D          ; 2
01B9 CD0000      CALL     GP0030
01BC E1          POP      H          ; 1
01BD 19          DAD      D
01BE 220400      SHLD     TD
63  1      IF((L<TD) AND (TD<U))THEN DO;
                                ; STATEMENT # 63
01C1 3A0700      LDA      L
01C4 CD0000      CALL     GP0094
01C7 9F          SBB      A
01C8 F5          PUSH     PSW          ; 1
01C9 3A0A00      LDA      U
01CC 110400      LXI      D,TD
01CF CD0000      CALL     GP0101
01D2 9F          SBB      A
01D3 C1          POP      B          ; 1
01D4 48          MOV      C,B
01D5 A1          ANA      C
01D6 1F          RAR
01D7 D20202      JNC      Q10
65  2      DO WHILE (N<THETA);
                                ; STATEMENT # 65
                                Q31:
01DA 210C00      LXI      H,THETA
01DD 3A0D00      LDA      N

```


66	3	01E0 BE 01E1 D2EE01	CMP M JNC Q32 CALL BKWD;		
					; STATEMENT # 66
67	3	01E4 CDA703	CALL BKWD THETA=THETA-1;		
					; STATEMENT # 67
68	3	01E7 210C00 01EA 35	LXI H,THETA DCR M END;		
					; STATEMENT # 68
69	2	01EB C3DA01	JMP Q31		
		Q32:	DO WHILE(N>THETA);		
					; STATEMENT # 69
		Q33:			
70	3	01EE 3A0C00 01F1 210D00 01F4 BE 01F5 D20202	LDA THETA LXI H,N CMP M JNC Q34 CALL FWD;		
					; STATEMENT # 70
71	3	01F8 CD5403	CALL FWD THETA=THETA+1;		
					; STATEMENT # 71
72	3	01FB 210C00 01FE 34	LXI H,THETA INR M END;		
					; STATEMENT # 72
73	2	01FF C3EE01	JMP Q33		
		Q34:	END;		
					; STATEMENT # 73
		Q10:			
74	1	IF(TD<L)THEN DO;			
					; STATEMENT # 74
76	2	0202 3A0700 0205 110400 0208 CD0000 020B D23F02	LDA L LXI D,TD CALL QP0101 JNC Q11 A=(A+ALT)/2;		
					; STATEMENT # 76
77	2	020E 3A0600 0211 210B00 0214 86 0215 5F 0216 1600 0218 210200 021B CD0000 021E 210B00 0221 73	LDA ALT LXI H,A ADD M MOV E,A MVI D,0 LXI H,2H CALL QP0029 LXI H,A MOV M,E IF(N=23)THEN N=24;		
					; STATEMENT # 77
		0222 3A0D00 0225 FE17 0227 C22F02	LDA N CPI 17H JNZ Q12		

```

                                ; STATEMENT # 78
                                022A 210D00 LXI H,N
                                022D 3618 MVI M,18H
                                @12:
79 2 N=N+A;
                                ; STATEMENT # 79
                                022F 3A0B00 LDA A
                                0232 210D00 LXI H,N
                                0235 86 ADD M
                                0236 77 MOV M,A
80 2 ALT=-ALT;
                                ; STATEMENT # 80
                                0237 3A0600 LDA ALT
                                023A 2F CMA
                                023B 3C INR A
                                023C 320600 STA ALT
81 2 END;
                                ; STATEMENT # 81
                                @11:
82 1 IF(TD>U)THEN DO;
                                ; STATEMENT # 82
                                023F 3A0A00 LDA U
                                0242 210400 LXI H,TD
                                0245 CD0000 CALL GP0103
                                0248 D27E02 JNC Q13
84 2 A=(ALT+A)/2;
                                ; STATEMENT # 84
                                024B 3A0B00 LDA A
                                024E 210600 LXI H,ALT
                                0251 86 ADD M
                                0252 5F MOV E,A
                                0253 1600 MVI D,0
                                0255 210200 LXI H,2H
                                0258 CD0000 CALL GP0029
                                025B 210B00 LXI H,A
                                025E 73 MOV M,E
85 2 ALT=-ALT;
                                ; STATEMENT # 85
                                025F 3A0600 LDA ALT
                                0262 2F CMA
                                0263 3C INR A
                                0264 320600 STA ALT
86 2 IF(N=27)THEN N=26;
                                ; STATEMENT # 86
                                0267 3A0D00 LDA N
                                026A FE1B CPI 1BH
                                026C C27402 JNZ Q14
                                ; STATEMENT # 87
                                026F 210D00 LXI H,N
                                0272 361A MVI M,1AH
                                @14:
88 2 N=N-A;
                                ; STATEMENT # 88
                                0274 210B00 LXI H,A
                                0277 3A0D00 LDA N
                                027A 96 SUB M
                                027B 320D00 STA N

```

```

89      2      END;
; STATEMENT # 89

      Q13:
90      1      IF(N<>THETA)THEN GOTO ITER;
; STATEMENT # 90

      027E 210C00      LXI      H,THETA
      0281 3A0D00      LDA      N
      0284 BE          CMP      M
      0285 CA8B02      JZ       Q15
; STATEMENT # 91
      0288 C38501      JMP      ITER
      Q15:

92      1      MAINT: CALL DELAY; /*10 SEC DELAY*/
; STATEMENT # 92
      MAINT:
      028B CD6703      CALL     DELAY
93      1      TD=INPUT(3); /*MEASURE DRYER TEMP*/
; STATEMENT # 93

      028E DB03      IN        3H
      0290 6F          MOV      L,A
      0291 2600      MVI      H,0
      0293 220400     SHLD     TD
94      1      DCR: IF((TD>U) AND (THETA>0)) THEN DO;
; STATEMENT # 94
      DCR:
      0296 3A0A00      LDA      U
      0299 210400      LXI      H,TD
      029C CD0000      CALL     GP0103
      029F 9F          SBB      A
      02A0 F5          PUSH     PSW      ; 1
      02A1 3E00      MVI      A,0H
      02A3 210C00      LXI      H,THETA
      02A6 96          SUB      M
      02A7 9F          SBB      A
      02A8 C1          POP      B      ; 1
      02A9 48          MOV      C,B
      02AA A1          ANA      C
      02AB 1F          RAR
      02AC D2B602      JNC      Q16
96      2      THETA=THETA-1;
; STATEMENT # 96
      02AF 210C00      LXI      H,THETA
      02B2 35          DCR      M
97      2      CALL FWD;
; STATEMENT # 97
      02B3 CD5403      CALL     FWD
98      2      END;
; STATEMENT # 98
      Q16:
99      1      INCR: IF((TD<L) AND (THETA<50)) THEN DO;
; STATEMENT # 99
      INCR:
      02B6 3A0700      LDA      L
      02B9 110400      LXI      D,TD
      02BC CD0000      CALL     GP0101

```

	02BF	9F	SBB	A	
	02C0	F5	PUSH	PSW	; 1
	02C1	3A0C00	LDA	THETA	
	02C4	D632	SUI	32H	
	02C6	9F	SBB	A	
	02C7	C1	POP	B	; 1
	02C8	48	MOV	C,B	
	02C9	A1	ANA	C	
	02CA	1F	RAR		
	02CB	D2D502	JNC	Q17	
101	2		CALL	FWD;	
					; STATEMENT # 101
	02CE	CD5403	CALL	FWD	
102	2			THETA=THETA+1;	
					; STATEMENT # 102
	02D1	210C00	LXI	H,THETA	
	02D4	34	INR	M	
103	2		END;		
					; STATEMENT # 103
		Q17:			
104	1		IF(INPUT(1)<=L)THEN GOTO SOLAR;		
					; STATEMENT # 104
	02D5	DB01	IN	1H	
	02D7	4F	MOV	C,A	
	02D8	3A0700	LDA	L	
	02DB	B9	CMP	C	
	02DC	DAE202	JC	Q18	
					; STATEMENT # 105
	02DF	C3D700	JMP	SOLAR	
		Q18:			
106	1		IF((TD>U) AND (THETA=0))THEN GO TO ALARM;		
					; STATEMENT # 106
	02E2	3A0A00	LDA	U	
	02E5	210400	LXI	H,TD	
	02E8	CD0000	CALL	QP0103	
	02EB	9F	SBB	A	
	02EC	F5	PUSH	PSW	; 1
	02ED	3A0C00	LDA	THETA	
	02F0	D600	SUI	0H	
	02F2	D601	SUI	1	
	02F4	9F	SBB	A	
	02F5	C1	POP	B	; 1
	02F6	48	MOV	C,B	
	02F7	A1	ANA	C	
	02F8	1F	RAR		
	02F9	D2FF02	JNC	Q19	
					; STATEMENT # 107
	02FC	C31F03	JMP	ALARM	
		Q19:			
108	1		IF((TD<L) AND (THETA=50))THEN GOTO ALARM;		
					; STATEMENT # 108
	02FF	3A0700	LDA	L	
	0302	110400	LXI	D,TD	
	0305	CD0000	CALL	QP0101	
	0308	9F	SBB	A	
	0309	F5	PUSH	PSW	; 1

```

030A 3A0C00 LDA THETA
030D D632 SUI 32H
030F D601 SUI 1
0311 9F SBB A
0312 C1 POP B ; 1
0313 48 MOV C,B
0314 A1 ANA C
0315 1F RAR
0316 D21C03 JNC Q20
; STATEMENT # 109
0319 C31F03 JMP ALARM
Q20:
110 1 GO TO MAINT;
; STATEMENT # 110
031C C38B02 JMP MAINT
111 1 ALARM: DO I=1 TO 10;
; STATEMENT # 111
ALARM:
031F 210900 LXI H,I
0322 3601 MVI M,1H
Q35:
0324 3E0A MVI A,0AH
0326 210900 LXI H,I
0329 BE CMP M
032A DA5203 JC Q36
112 2 CALL CO('E');
; STATEMENT # 112
032D 0E45 MVI C,45H
032F CD0000 CALL CO
113 2 CALL CO('R');
; STATEMENT # 113
0332 0E52 MVI C,52H
0334 CD0000 CALL CO
114 2 CALL CO('R');
; STATEMENT # 114
0337 0E52 MVI C,52H
0339 CD0000 CALL CO
115 2 CALL CO('O');
; STATEMENT # 115
033C 0E4F MVI C,4FH
033E CD0000 CALL CO
116 2 CALL CO('R');
; STATEMENT # 116
0341 0E52 MVI C,52H
0343 CD0000 CALL CO
117 2 CALL CO(' ');
; STATEMENT # 117
0346 0E20 MVI C,20H
0348 CD0000 CALL CO
118 2 END;
; STATEMENT # 118
034B 210900 LXI H,I
034E 34 INR M
034F C22403 JNZ Q36
Q36:

```

119 1 END USDA;

0352 FB
0353 76EI
HLT

; STATEMENT # 119

MODULE INFORMATION:

CODE AREA SIZE	= 03BAH	954D
VARIABLE AREA SIZE	= 000EH	14D
MAXIMUM STACK SIZE	= 0006H	6D
127 LINES READ		
0 PROGRAM ERROR(S)		

END OF PL/M-80 COMPILATION



GEORGIA INSTITUTE OF TECHNOLOGY
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April 18, 1980

Dr. James L. Butler
Coastal Plain Experiment Station
Tifton, GA 31794

Dear Jim:

Enclosed please find the April 1980 quarterly report. I look forward to seeing you on Thursday, April 24.

Sincerely,

Jay H. Schlag, Ph.D.

JHS:lso

Enclosures

QUARTERLY REPORT

Submitted to the
Department of Energy
Through the U.S. Department of Agriculture

from
Georgia Institute of Technology
225 North Avenue, N.W.
Atlanta, Georgia 30332

CONTROL SYSTEMS FOR INTERFACING SOLAR AND
BIOMASS FUELS IN AGRICULTURAL DRYERS

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April 1980

Part of the past quarter's work on the hot air mixing system has involved investigation of a suitable method for providing heated air for the prototype unit. One alternative includes a helical spiral of copper tubing to encircle the input air path. The copper tubing would carry the biomass fuel of interest (e.g. methane) and would be perforated at intervals to allow a series of gas flames. Thus the input air would be heated as it flowed into the system. Another alternative consists of a large cubical enclosure in which space heaters would be placed and from which the heated air would be drawn. Still another, and possibly the best, air heating method would use standard furnace grating technology. The valve and ignition system would be controlled together and activated by a single voltage. The advantage in using standard furnace equipment for the prototype unit is that the component parts necessary for an actual solar/biomass agricultural dryer would then be easily available, off-the-shelf items, which would presumably be less expensive than a custom-made system.

Another object of last quarter's effort was the microprocessor control for the hot air mixing system. The 8020 microprocessor unit was connected to the pipe-and-valve system and was used to control the stepping motor which opens and closes the valves in the two air channels. The temperature sensors provided inputs to the computer, and the alarm indicator lights were functional. In addition, the microprocessor software has been modified to provide more interaction with the operator. An ADM-3A CRT terminal has been interfaced to the microprocessor so that the program can output messages which indicate what part of the program is currently being executed. Another aid to prototype testing that has been added is the facility for downloading programs from the MDS-230 development system to the 8020 microprocessor unit. This has eliminated much of the time involved in program development and debugging. With this capability, the software can be loaded into RAM, making it possible for the operator to set breakpoints within the program.

A complete listing of the PLM 80 program is included along with explanatory comments.

ISIS-II PL/M-86 V3.0 COMPILATION OF MODULE USDA
 OBJECT MODULE PLACED IN :F1:USDA.OBJ
 COMPILER INVOKED BY: PLM86 :F1:USDA.SRC

```

1      USDA:DO;          /*DATE:11 APRIL 80*/
2      1      DECLARE OE4 BYTE INITIAL(0FFH);
3      1      DECLARE (I,U,TS,TA,TD) ADDRESS INITIAL(700,900);
4      1      DECLARE (ALT,J,I,A,THETA,N) BYTE INITIAL(1,0,0,0,0,0);
5      1      DECLARE KS(50) ADDRESS DATA(3282,1689,1157,891,731,624,547,43
        408,378,353,331,313,296,282,269,258,247,238,229,221,
        213,206,200,194,188,183,178,173,168,163,159,154,151,147,
        143,140,136,132,129,126,122,119,116,113,109,106,103,100);
6      1      DECLARE KA(50) ADDRESS DATA(100,103,106,109,113,116,119,122,1
        132,136,140,143,147,151,155,159,163,168,173,178,183,188,1
        200,206,213,221,229,238,247,258,269,282,296,313,331,353,3
        408,444,489,547,634,731,892,1157,1639,3282);

7      1      CO:PROCEDURE(CHAR) EXTERNAL;
8      2      DECLARE CHAR BYTE;
9      2      END CO;

10     1      NMOUT:PROCEDURE(ASCII) EXTERNAL;
11     2      DECLARE ASCII BYTE;
12     2      END NMOUT;

13     1      FWD:PROCEDURE; /*PULSES THE MOTOR CONTROL THAT
        OPENS THE SOLAR DAMPER(1.6DEG/PULSE)*/

14     2      OE4=OE4 AND 0EFH; /*SET BIT 4--PORT E4
        HAS INVERTED OUTPUTS*/
15     2      OUTPUT(0E4H)=OE4;
16     2      DO I=1 TO 50;
17     3      CALL TIME(100); /*10 MS DELAY*/
18     3      END;
19     2      OE4=OE4 OR 10H; /*ZERO BIT 4*/
20     2      OUTPUT(0E4H)=OE4;
21     2      DO I=1 TO 50;
22     3      CALL TIME(100);
23     3      END;
24     2      END FWD;

25     1      DELAY:PROCEDURE;
26     2      DO I=1 TO 4;
27     3      DO J=1 TO 250; /*10 SEC DELAY*/
28     4      CALL TIME(100);
29     4      END;
30     3      END;
31     2      END DELAY;

/*THE FOLLOWING PROCEDURE OPENS SOLAR DAMPER TO MAX POSITION(0E6H)

32     1      DEG92:PROCEDURE;
33     2      DO WHILE(SHR((NOT INPUT(0E6H)),1));
34     3      CALL FWD;
35     3      END;
```

```

36      2      END DEG90;

37      1      BKWD:PROCEDURE;      /*PULSES MOTOR CONTROL TO
                                   CLOSE SOLAR DAMPER(1.0DEG/PULSE)*/

78      2      OE4=OE4 AND 0F7H;    /*SET BIT 3*/
39      2      OUTPUT(0E4H)=OE4;    /*RAISE CONTROL LINE
                                   FOR BK(CW) PULSES*/

40      2      DO I=1 TO 50;
41      3      CALL TIME(100);      /*10 MS DELAY*/
42      3      END;
43      2      OE4=OE4 OR 8H;        /*ZERO BIT 3*/
44      2      OUTPUT(0E4H)=OE4;    /*LOWER CONTROL LINE*/
45      2      DO I=1 TO 50;
46      3      CALL TIME(100);
47      3      END;
48      2      END BKWD;

49      1      INIT:OE4=0F7H;        /*INITIALIZE CONTROL WORD
                                   FOR PORT E4*/

50      1      OUTPUT(0E3H)=9EH;
51      1      OUTPUT(0E7H)=80H;

52      1      START:DO WHILE (NOT INPUT(0E6H));/*CLOSE DAMPER TO SOLAR WIP*/
53      2      CALL BKWD;
54      2      END;

55      1      SOLAR:OE4=(0F8H AND OE4) OR 5;
56      1      OUTPUT(0E4H)=OE4;    /*SELECT SOLAR TEMP SENSOR*/
57      1      OUTPUT(0EAH)=1;
58      1      OUTPUT(0EAH)=0;      /*PULSE TO INITIATE CONVERSION*/
59      1      CALL CO(0AH);
60      1      CALL CO(0DH);
61      1      CALL CO('S');
62      1      CALL CO('O');
63      1      CALL CO('I');
64      1      CALL CO('A');
65      1      CALL CO('R');
66      1      CALL CO(0DH);
67      1      CALL CO(0AH);
68      1      TS=(0C2H AND INPUT(0EAH))*4+(NOT INPUT(0E6H));

                                   /*TS=SOLAR TEMP*/

69      1      CALL NMOUT(HIGH(TS));
70      1      CALL NMOUT(LOW(TS));
71      1      CALL CO(' ');
72      1      CALL CO('T');
73      1      CALL CO('S');
74      1      CALL CO(0DH);
75      1      CALL CO(0AH);
76      1      IF(TS>0)THEN GOTO MIX;
78      1      CALL DEG90;          /*TS<0,OPEN SOLAR DAMPER MAX*/

79      1      IF(TS<L)THEN GOTO BURNER;

```

```

81      1      ELSE CALL DELAY;      /*ELSE L<TS<U;
82      1      GOTO SOLAR;          STAY IN SOLAR ROUTINE*/

83      1      BURNER: OF4=(OE4 AND 2D8H) OR 6;
84      1      OUTPUT(0E4H)=OE4;      /*SELECT DRYER TEMP SENSOR AND
85      1      RAISE CONTROL LINE TO LIGHT BURNER*/
86      1      INTCON: OUTPUT(0EAH)=1;
87      1      OUTPUT(0EAH)=0;      /*INITIATE CONVERSION*/
88      1      CALL CO('B');
89      1      CALL CO('U');
90      1      CALL CO('R');
91      1      CALL CO('N');
92      1      CALL CO('E');
93      1      CALL CO('R');
94      1      CALL CO(0DH);
95      1      CALL CO(0AH);
96      1      TD=(0C0H AND INPUT(0EAH))*4+(NOT INPUT(0EBH));
97      1      /*TD=DRYER TEMP*/
98      1      CALL NMOUT(HIGH(TD));
99      1      CALL NMOUT(LOW(TD));
100     1      CALL CO(' ');
101     1      CALL CO('T');
102     1      CALL CO('D');
103     1      CALL CO(0DH);
104     1      CALL CO(0AH);

105     1      IF (TD<L+(U-L)/2) THEN CALL DELAY;
106     1      ELSE GO TO BRNOFF;
107     1      GO TO INTCON;
108     1      BRNOFF: OE4=OE4 OR 20H;      /*ZERO BIT 5 OF PORT1*/
109     1      OUTPUT(0E4H)=OE4;      /*TURN OFF BURNER*/

110     1      LOOP:   OE4=(OE4 AND 2F8H) OR 5;
111     1      OUTPUT(0E4H)=OE4;      /*SELECT TS*/
112     1      OUTPUT(0EAH)=1;
113     1      OUTPUT(0EAH)=0;
114     1      CALL CO('L');
115     1      CALL CO('O');
116     1      CALL CO('O');
117     1      CALL CO('P');
118     1      CALL CO(0AH);
119     1      CALL CO(0DH);
120     1      TS=(0C0H AND INPUT(0EAH))*4+(NOT INPUT(0EBH));
121     1      CALL NMOUT(HIGH(TS));
122     1      CALL NMOUT(LOW(TS));
123     1      CALL CO(' ');
124     1      CALL CO('T');
125     1      CALL CO('S');
126     1      CALL CO(0DH);
127     1      CALL CO(0AH);
128     1      IF (TS<L)THEN CALL DELAY;
129     1      ELSE GOTO SOLAR;
130     1      OE4=(OE4 AND 2F8H) OR 6;

```

```

131 1      OUTPUT(0E4H)=0E4;          /*SELECT TD*/
132 1      OUTPUT(0E4H)=1;
133 1      OUTPUT(0E4H)=0;
134 1      CALL TIME(100);
135 1      TD=(0C0H AND INPUT(0E4H))*4+(NOT INPUT(0E5H));
136 1      CALL NMOUT(HIGH(TD));
137 1      CALL NMOUT(LOW(TD));
138 1      CALL CO(' ');
139 1      CALL CO('T');
140 1      CALL CO('D');
141 1      CALL CO(0DH);
142 1      CALL CO(0AH);
143 1      IF(TD<L)THEN GOTO BURNER; /*IF TD<L & TS<L*/
145 1      ELSE GOTO LOOP; /*IF TD>L & TS<L*/

146 1      MIX:  OUTPUT(0E4H)=(0E4 OR 07H); /*SELECT AMBIENT
                                TEMP SENSOR*/
147 1      OUTPUT(0E4H)=1;
148 1      OUTPUT(0E4H)=0;
149 1      CALL TIME(100);
150 1      TA=(0C0H AND INPUT(0E4H))*4+(NOT INPUT(0E5H));

/*TA=AMBIENT TEMP*/

151 1      CALL CO('M');
152 1      CALL CO('I');
153 1      CALL CO('X');
154 1      CALL CO(0AH);
155 1      CALL CO(0DH);
156 1      CALL NMOUT(HIGH(TA));
157 1      CALL NMOUT(LOW(TA));
158 1      CALL CO(' ');
159 1      CALL CO('T');
160 1      CALL CO('A');
161 1      CALL CO(0DH);
162 1      CALL CO(0AH);

/*CHECK DAMPER POSITION; IF FULLY OPEN, THETA=50*/

163 1      IF((INPUT(0E5H) AND 1)=1)THEN THETA=0;
165 1      IF((INPUT(0E5H) AND 2)=2)THEN THETA=50;

/*ITERATIVE PROCEDURE FOR DETERMINING
THEORETICAL SETTING ,GIVEN TS & TD*/

167 1      N,A=25;
168 1      ALT=1;
169 1      CALL CO('I');
170 1      CALL CO('T');
171 1      CALL CO('E');
172 1      CALL CO('R');
173 1      CALL CO(0DH);
174 1      CALL CO(0AH);
175 1      ITER:  TD=(TS*10/KS(N)+TA*10/KA(N))*10;
176 1      IF((L<TD) AND (TD<U))THEN DO;
178 2          DO WHILE (M<THETA);
179 3          CALL BKWD;

```

```

180 2          THETA=THETA-1;
181 3          END;
182 2          DO WHILE(N>THETA);
183 3          CALL FWD;
184 3          THETA=THETA+1;
185 3          END;
186 2          END;

```

```

187 1          IF(TD<L) THEN DO;
188 2              A=(A+ALT)/2;
189 2              IF(N=23) THEN N=24;
190 2              N=N+A;
191 2              ALT=-ALT;
192 2              END;
193 1          IF(TD>U) THEN DO;
194 2              A=(ALT+A)/2;
195 2              ALT=-ALT;
196 2              IF(N=27) THEN N=26;
197 2              N=N-A;
198 2              END;
199 1          IF(N<>THETA) THEN GOTO ITER;

```

/*THIS ROUTINE WILL MAINTAIN THE CORRECT DAMPER SETTING
FOR THE DESIRED DRYER TEMPERATURE*/

```

205 1          MAINT: OF4=(OF4 AND OF8H) OR 6;
206 1          OUTPUT(OF4H)=OF4;          /*SELECT TD*/
207 1          OUTPUT(OF4H)=1;
208 1          OUTPUT(OF4H)=0;
209 1          CALL CO('M');
210 1          CALL CO('A');
211 1          CALL CO('I');
212 1          CALL CO('N');
213 1          CALL CO('T');
214 1          CALL CO(OF4H);
215 1          CALL CO(OF4H);
216 1          CALL DELAY;          /*10 SEC DELAY*/

```

/*MEASURE DRYER TEMP*/

```

217 1          TD=(OC0H AND INPUT(OF4H))*4+(NOT INPUT(OF8H));
218 1          CALL NMOUT(HIGH(TD));
219 1          CALL NMOUT(LOW(TD));
220 1
221 1          CALL CO(' ');
222 1          CALL CO('T');
223 1          CALL CO('D');
224 1          CALL CO(OF4H);
225 1          CALL CO(OF4H);

```

/*THE FOLLOWING ROUTINES COMPENSATE FOR ANY POSSIBLE INACCURACIES
IN THE THEORETICAL CALCULATION FOR THE DAMPER SETTING*/

```

226 1          DCR: IF((TD>U) AND (THETA>0)) THEN DO;
227 2              THETA=THETA-1;
228 2              CALL FWD;
229 2              END;

```

```

132 1      INCR:  IF((TD<L) AND (THETA<50)) THEN DO;
132 2          CALL FWD;
133 2          THETA=THETA+1;
134 2          END;
135 1      OR4=(OE4 AND 0F8H) OR 5;
136 1      OUTPUT(0E4H)=OR4;      /*SELECT TS*/
137 1      OUTPUT(0EAH)=1;
138 1      OUTPUT(0EAH)=0;
139 1      CALL TIME(100);
140 1      TS=(0C0H AND INPUT(0EAH))*4+(NOT INPUT(0EBH));
141 1      CALL NMOUT(HIGH(TS));
142 1      CALL NMOUT(LOW(TS));
143 1      CALL CO(' ');
144 1      CALL CO('T');
145 1      CALL CO('S');
146 1      CALL CO(0AH);
147 1      CALL CO(0DH);

/*THIS ROUTINE WILL MAINTAIN DESIRED DRYER TEMP INDEFINITELY
UNLESS SOLAR TEMP DROPS BELOW LOWER LIMIT;
IN WHICH CASE, PROGRAM RETURNS TO SOLAR ROUTINE*/

242 1      IF(TS<=L)THEN GOTO SOLAR;

/*IF THE DRYER COMPARTMENT BECOMES TOO HOT OR TOO COOL,
AND THE DAMPER IS AT MIN OR MAX SETTING RESPECTIVELY.
AN ALARM LIGHT WILL BE ACTIVATED AND THE PROGRAM HALTED*/

250 1      IF((TD>U) AND (THETA=0))THEN GO TO ALARM;
252 1      IF((TD<L) AND (THETA=50))THEN GOTO ALARM;

254 1      GO TO MAINT;

255 1      ALARM:  OR4=OE4 AND 0FFH;      /*SET ALARM BIT*/
256 1      OUTPUT(0E4H)=OR4;      /*RAISE ALARM LINE*/
257 1      END USDA;

```

MODULE INFORMATION:

```

CODE AREA SIZE      = 0706H      1792D
VARIABLE AREA SIZE  = 0011H      17D
MAXIMUM STACK SIZE  = 0006H      6D
315 LINES READ
0 PROGRAM ERROR(S)

```

END OF PL/M-80 COMPILATION

E-21-662

FINAL REPORT

**CONTROL SYSTEMS FOR INTERFACING
SOLAR AND BIOMASS FUELS IN AGRI-
CULTURAL DRYERS**

Principal Investigator:

**Dr. J. H. Schlag
Professor**

Project Manager:

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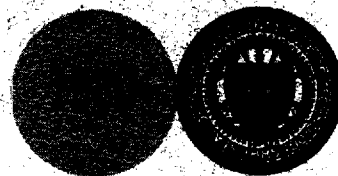
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SCHOOL OF ELECTRICAL ENGINEERING
ATLANTA, GEORGIA 30332



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TABLE OF CONTENTS

	<u>page</u>
I. INTRODUCTION	1
II. THE MODEL	
A. Introduction	4
B. Definition of Symbols	6
C. Explanation of Model	7
III. THE MICROPROCESSOR CONTROL SYSTEM	14
IV. THE CONTROL ALGORITHM	18
V. SOFTWARE	23
VI. EXPERIMENTAL PROCEDURE	26
VII. RESULTS AND CONCLUSIONS	31
APPENDIX A: DETAILED FLOWCHARTS FOR CONTROLLING DAMPERS AND BURNERS . .	32
APPENDIX B: PROGRAM LISTING	38
APPENDIX C: REFERENCES	68

TABLE OF FIGURES

FIGURE 1: Process Control System	5
FIGURE 2: Circuit Diagram	11
FIGURE 3: Microprocessor Control System	15
FIGURE 4: Experimental vs. Calculated Airflow .	21
FIGURE 5: Controller Flow Chart	24
FIGURE 6: T_s , T_d , and θ as Functions of Time During a Test of the Controller Program	28

TABLE OF FIGURES (CONTINUED)

	<u>page</u>
FIGURE 7: Relationship of Drying Temperature and State of Burner over Time During a Test of the Burner Loop	29
FIGURE 8: Temperature of Burner-Heated Air vs. Time from Switch-On	30

I. INTRODUCTION

Previous work has shown that solar energy is a feasible alternative to fossil fuels for heating air used in crop drying. However, the greatest drawback to solar energy is that it is not continuously available, and other energy sources must be used as backup. Research is being conducted into the use of biomass to generate methane and alcohol which could be used as backup fuels for solar dryers. In order to interface direct solar-heated air, ambient air, and auxiliary biomass-fueled heat, some means of intelligent process control is required for optimum energy performance. At one time this would have necessitated access to a large computing facility, having many capabilities in addition to the control function needed. Now, however, microprocessor technology has provided smaller units of computing power so that a relatively inexpensive microprocessor of more limited ability can be dedicated to a single task. The application of a microprocessor to the interfacing problem, together with modeling and construction of the air-mixing system, was the overall objective of this work.

There are several reasons why solar energy and intelligent microprocessor control represent important innovations for agricultural drying. The need for abundant, inexpensive energy for drying is demonstrated in several ways. The largest quantities of energy for agricultural drying in Georgia and the

Southeast are presently consumed on the peanut and tobacco crops, with peanuts valuable both as a direct source of protein and indirectly as a feed for domestic animals. In addition, growing demand for forage crops to replace grain as food for cattle will result in expanded drying operations. As continuing growth in the world population causes increased demand for low-cost protein, the importance of these feed crops especially suited to the southeastern United States will rise. Thus, the production of peanuts, tobacco, and forage crops alone would be significantly assisted by the low-cost availability of solar-powered dryers.

Furthermore, the detailed requirements of optimum crop drying indicate the careful monitoring of temperature that a microprocessor control system can provide. For example, peanuts must be dried quickly enough to avoid the growth of mold, one type of which produces a rather toxic carcinogen called aflatoxin. The aflavus mold enters any nut with cracks and grows favorably at about 77°F. If the moisture level is reduced below 10%, the mold will not form. On the other hand, peanuts dried at temperatures much above 90°F in conventional dryers become bitter and bring lower market prices. For these reasons, drying chamber temperatures for peanuts must be carefully controlled.

Another example of the complexity of the drying process is shown by tobacco, one of the three largest cash crops and the

largest user of agricultural process energy in Georgia. It requires substantial heat input for curing and drying with as much as 400-500% of the final tobacco weight being water before curing. Tobacco curing is additionally complicated because the leaves are "living" matter when the process begins and require careful attention if the final cured product is to be of high quality.

Finally, even the drying of forage should be performed in a temperature-controlled setting, so that nutritional value is maximized and oxidation and browning minimized. Thus the various requirements which must be met in agricultural drying indicate the need for alternative energy sources and intelligent automatic control, as provided by a microprocessor system.

II. THE MODEL

A. Introduction

The work on this project began with the design of a mathematical model of the drying process; the primary source of heat energy was taken to be solar-heated air supplied by conventional collectors. The temperature of this solar-heated air would be lowered, when necessary, by mixing with ambient air; it would be raised, when necessary, by the addition of biomass-fueled heat energy. The microprocessor would receive measurements of various temperatures and use these values to make decisions governing the operational modes of the drying system. Parts of the model would thus be implemented in developing the algorithms used by the microprocessor in the decision process. After construction of the prototype system, partial verification of the model was performed experimentally.

The process control system is shown in Figure 1. The valves to ambient air and the solar collectors are controlled by the microprocessor, as is the biomass gas inlet. The inputs to the microprocessor are ambient air temperature, solar collector temperature, and drying chamber temperature; the outputs are the controls on the valve openings and gas inlet. The model which was developed is essentially a static description of the relationships involved. However, because of the large time-span involved in drying crops (of the order of 24 hours)

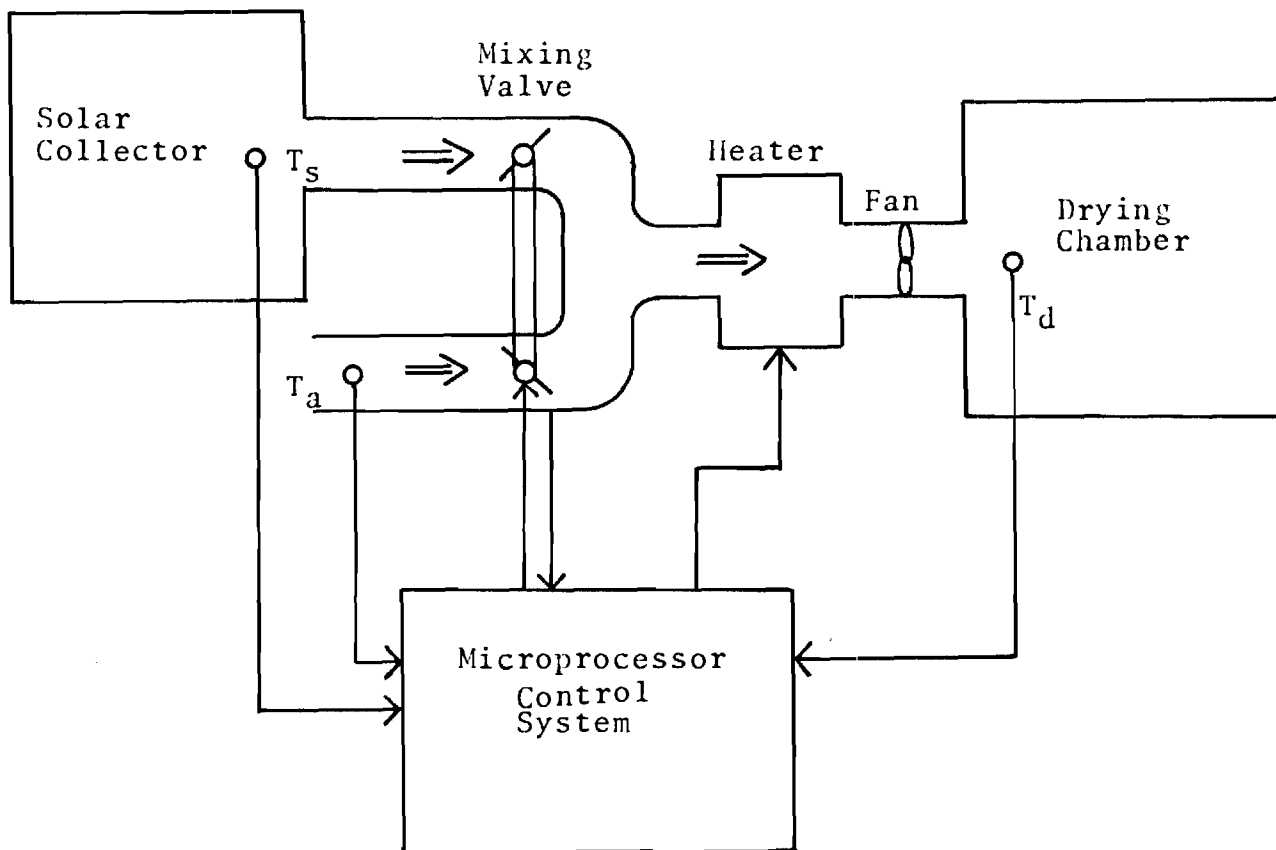


FIGURE 1. Process Control System

and the slow response time of valve mechanisms, static relationships can be employed by the microprocessor in an iterative manner, effectively producing a slow-dynamic model.

The first question addressed by the model is how the ideal drying temperature for a particular substance determines the length of time required to bring the moisture content from some initial level to a predetermined final level.

The second question addressed is what combination of ambient air, solar-heated air, and additional biomass thermal energy is most appropriate and economical under prevailing climatic conditions, i.e., ambient temperature, insolation, etc.

Finally the desired rates of flow of ambient air and solar-heated air must be related to the angular openings of the two valves and to any resistance to air flow (drag) inherent in the two sources.

B. Definition of Symbols

Let symbols be defined as follows:

Q_{req} = heat energy required for drying

Q_{sup} = heat energy supplied by ambient air, solar collectors, biomass fuel, or some combination of these three

m = mass of matter to be dried

M = mass of air used in drying

u_i = initial water fraction in matter to be dried

u_f = final water fraction in matter to be dried

c_w = specific heat capacity of water = 1.0 Kcal/KgC⁰
 c_a = specific heat capacity of ambient air
 h_v = heat of vaporization of water at the drying temperature
 h_c = heat of combustion of biomass fuel
 T_a = temperature (°C) of ambient air
 T_s = temperature of solar collector system
 T_d = ideal drying temperature for a particular type of matter
 T_m = initial temperature of matter to be dried
 T_i = temperature of warm air before heating by biomass fuel
 p_a = density of ambient air
 \dot{v}_d = total volume flow rate provided by fan, assumed constant
 \dot{v}_a = volume flow rate of ambient air
 \dot{v}_s = volume flow rate of solar-heated air
 Dt = time duration of drying process
 \dot{q}_{req} = thermal power required from biomass fuel
 \dot{q}_{sup} = thermal power supplied by biomass fuel
 \dot{v} = volume flow rate for gas in the biomass heater
 θ = angle of opening of valve to solar collector system
 ϕ = angle of opening of valve to ambient air
 r = radius of duct pipe

C. Explanation of Model

From a consideration of the expressions for \dot{Q}_{req} and \dot{Q}_{sup} the relation between T_d and Dt can be shown:

$$Q_{\text{req}} = (u_i - u_f)m c_w(T_d - T_m) + (u_i - u_f)m h_v \quad (1)$$

$$\begin{aligned} Q_{\text{sup}} &= M c_a T_d \\ &= p_a \dot{v}_d Dt c_a T_d \end{aligned} \quad (2)$$

By recognizing that Q_{sup} must equal Q_{req} , and that p_a , \dot{v}_d , and c_a are not adjustable, it follows that T_d determines Dt .

The discussion now concerns how usage of ambient air, solar-heated air and biomass fuel is determined.

Case 1: If $T_a < T_d$ and $T_s = T_d$, then open only the valve to the solar collectors, leaving valve to ambient air closed and biomass heater off. In this case $\dot{v}_s = \dot{v}_d$, and $\dot{v}_a = 0$.

Case 2: If $T_a < T_d$ and $T_s > T_d$, then leave biomass heater off and open both valves (to ambient air and solar collectors) to appropriate degrees so that

$$\begin{cases} \dot{v}_a + \dot{v}_s = \dot{v}_d \\ T_a \dot{v}_a + T_s \dot{v}_s = T_d \dot{v}_d \end{cases} \quad (3)$$

whose solution is

$$\dot{v}_a = \dot{v}_d \left(\frac{T_s - T_d}{T_s - T_a} \right) \quad \dot{v}_s = \dot{v}_d \left(\frac{T_d - T_a}{T_s - T_a} \right) \quad (4)$$

Case 3: Finally, if $T_a < T_d$ and $T_s < T_d$, then extra heat energy will have to be added by the biomass-powered heater.

In this case:

$$\begin{aligned}\dot{v}_a + \dot{v}_s &= \dot{v}_d \\ T_a \dot{v}_a + T_s \dot{v}_s &= T_i \dot{v}_d < T_d \dot{v}_d\end{aligned}\tag{5}$$

$$\text{and } T_i < T_d$$

In order to raise T_i to T_d , \dot{q}_{req} Kcal/sec must be added, where

$$\begin{aligned}\dot{q}_{\text{reg}} &= \frac{d}{dt} \left(M c_a (T_d - T_i) \right) \\ &= c_a (T_d - T_i) \rho_a \dot{v}_d\end{aligned}\tag{6}$$

The thermal power supplied is given by

$$\dot{q}_{\text{sup}} = h_c \dot{v}\tag{7}$$

Since \dot{q}_{sup} must equal \dot{q}_{req} , T_i determines \dot{v} .

Although there will be a thermocouple positioned to measure the temperature T_i of the air mixed from the ambient air valve and the solar system valve, it is a simple matter to calculate it from T_s , T_a , \dot{v}_a , and \dot{v}_s .

$$T_i = \frac{T_a \dot{v}_a + T_s \dot{v}_s}{\dot{v}_a + \dot{v}_s} \quad (8)$$

Even though it is intuitively apparent in this form as a weighted average, the expression can also be found by using a simple heat transfer calculation.

It remains to discuss how the volume flow rate for a valve depends on angular opening and on any resistive structures within. When the two valves are used together, these flow rates will be coupled, as stated earlier.

$$\dot{v}_a + \dot{v}_s = \dot{v}_d$$

It will be useful to consider an analogous electrical circuit. Let the resistance within the ambient air system be R_a , that within the solar system be R_s . Let the resistance offered by the solar system valve (open to angle θ) be R_θ , that offered by the ambient air valve (open to angle ϕ) be R_ϕ . Let the total air flow rate \dot{v}_d be represented by the total current in the circuit i_d , and the flow rates in the "parallel" valves by i_a and i_s . The source of emf (pressure) is E . A diagram of the circuit is given in Figure 2. The solutions to this circuit for $i_a(\dot{v}_a)$ and $i_s(\dot{v}_s)$ are given by:

$$i_a = i_d \left(\frac{R_s + R_\theta}{R_a + R_\phi + R_s + R_\theta} \right) \quad (9a)$$

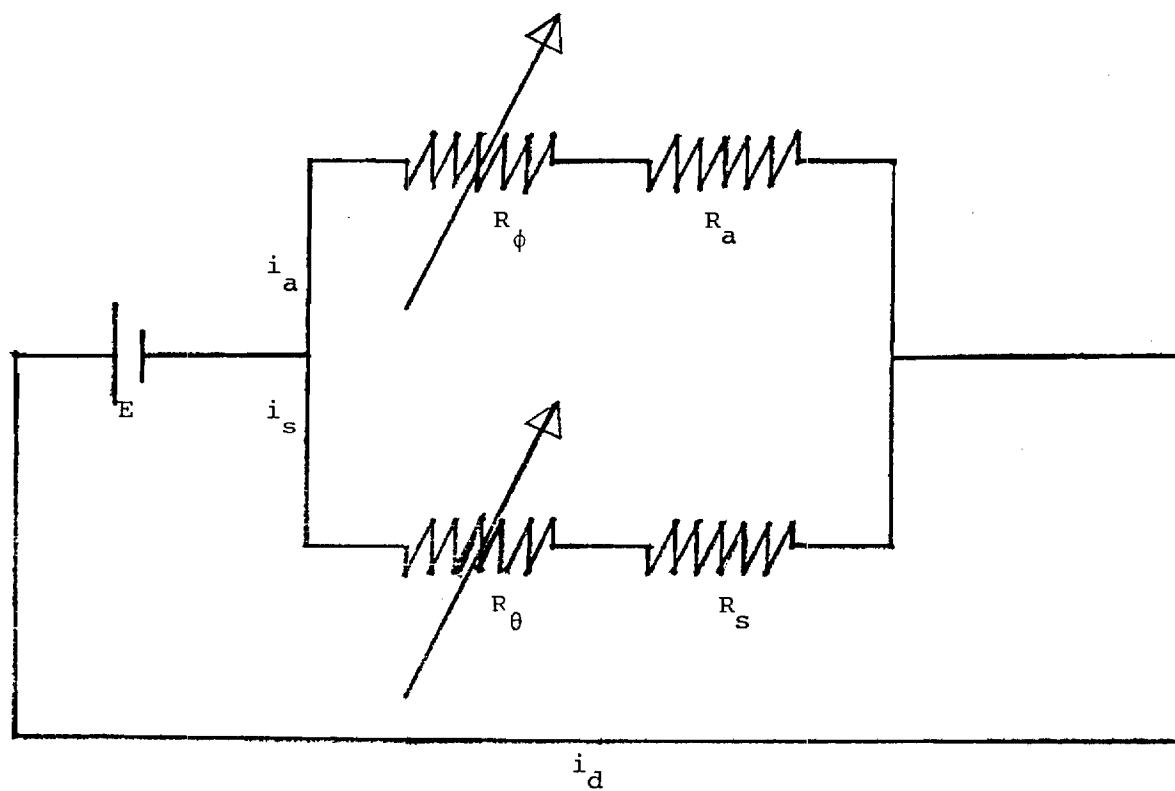


FIGURE 2
CIRCUIT DIAGRAM

$$i_s = i_d \left(\frac{R_a + R_\phi}{R_a + R_\phi + R_s + R_\theta} \right) \quad (9b)$$

It is clear from the solutions to this analogous electrical circuit that the drag factors in the two air paths of the drying system would be closely coupled. Since there is no a priori way of modeling the air drag quantities represented by R_a , R_ϕ , R_s , and R_θ , empirical measurements would be used to obtain their relative magnitudes. One useful relationship can be obtained, however. It seems reasonable that the amount of drag presented to the air flow by a valve would be proportional to the projected area of the valve on the plane of the opening; thus

$$R_\phi \propto \pi r^2 \cos \phi \quad \text{and} \quad R_\theta \propto \pi r^2 \cos \theta \quad (10)$$

where it is assumed that the radius of the duct pipe r will be the same throughout the system. Nevertheless, an exact understanding of the magnitudes of these four drag factors will not be necessary because of the iterative control procedure employed: an initial setting of the air valves and gas inlet will be determined by the input parameters; the intermediate temperature and ultimate drying temperature will be checked; the air valves and gas inlet will be re-set, if necessary; then temperatures will be re-checked and the iteration process continued.

It will be shown in subsequent sections of this report that only certain parts of this model were needed in the microprocessor algorithm and that certain adaptations were made in order to facilitate programming. Also, the postulated cosine dependence of flow resistance (drag) with respect to angle of opening was tested experimentally, with graphical comparison of results.

III. THE MICROPROCESSOR CONTROL SYSTEM

The microprocessor based control system, as shown in Figure 3, contains an Intel 80/20 microprocessor, an Intersil 7901 A/D converter, three LM3911 temperature sensors, a Slo-Syn stepping motor, and a Slo-Syn stepping motor controller. The three temperature transducers are used to measure the solar temperature, T_s , the ambient temperature, T_a , and the drying temperature, T_d . These three temperatures are selected by the microprocessor through the multiplexer, and converted to digital form by the A/D converter.

The microprocessor then compares the three temperatures and decides whether to increase or decrease the relative amount of solar versus ambient air. The microprocessor increases or decreases the relative flow by sending pulses and direction to the stepping motor controller, which, in turn, sends the stepping motor in either a clockwise or a counterclockwise direction depending on the direction level from the microprocessor. The stepping motor is connected to the vanes in the flow of solar and ambient air, so that as the solar vanes are opened the ambient air vanes are closed, and vice versa.

A brief description of each component of the system follows. The LM3911 temperature transducers are commercially available integrated circuits that develop a voltage linearly proportional to temperature in degrees Kelvin. They have an approximate

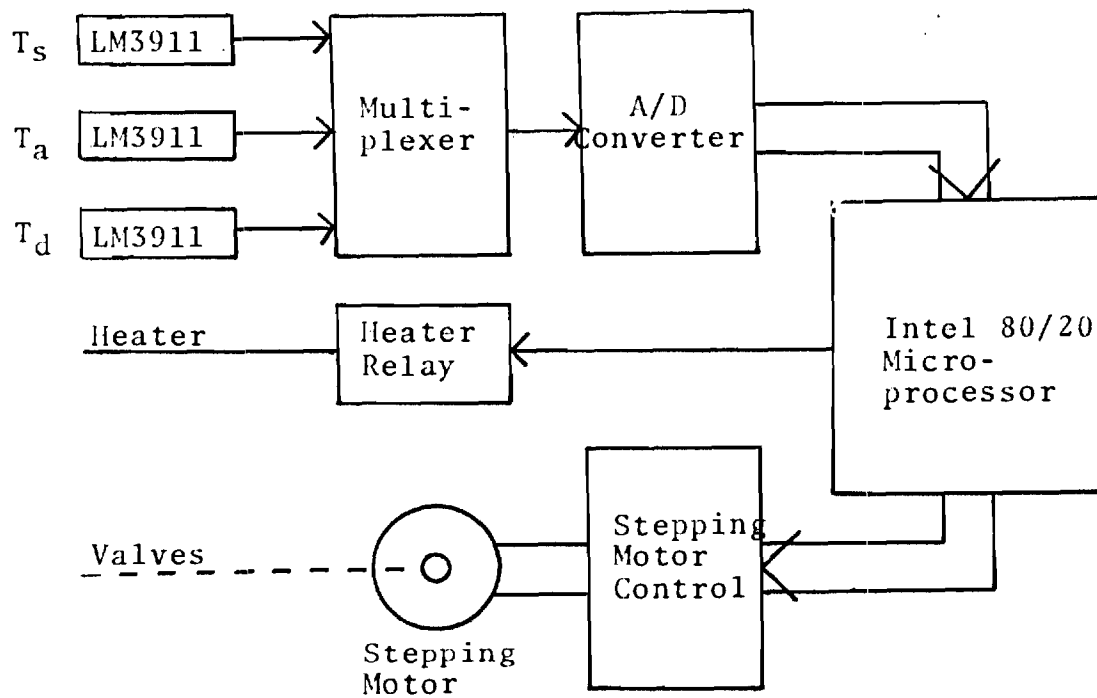


FIGURE 3. Microprocessor Control System

sensitivity of $10 \text{ mV}/^{\circ}\text{K}$ over an operating temperature range from 248°K to 358°K or -25°C to $+85^{\circ}\text{C}$. The outputs from the temperature transducers are converted from degrees Kelvin to degrees Centigrade by using a simple offset operational amplifier circuit with an LM308 operational amplifier.

The multiplexer is a Datel model #MM-8, solid state multiplexer using FET switches and integral TTL-compatible decoding. This unit can be connected directly to the output of the Intel microprocessor, so that any one of the three temperature transducers can be selected by a binary code sent from the microprocessor.

The analog-to-digital (A/D) converter is used to convert the output from the multiplexer into a binary form for input to the microprocessor system. This unit has 12 bits of output and has an accuracy of $\pm 1 \text{ mV}$.

The microprocessor system is an Intel SBC 80/20, single board computer with an 8080 microprocessor, two kilobytes of random-access memory (RAM), four kilobytes of EPROM memory, 48 lines of digital input or output, asynchronous serial I/O port, and a real time clock. The EPROM memory is used to hold the program that executes the control algorithm on the 8080 microprocessor. The random-access memory is used as a "scratch pad" to hold data for the control algorithm. Digital output lines are used to control the multiplexer, A/D conversion, and stepping motor control. Digital inputs are used for the input

of temperature data. The serial I/O board is used in conjunction with a CRT terminal to print out the status of the controller algorithm at points for debugging and diagnostic purposes. The real time clock is used for generating real time delays in the control algorithm program.

The Slo-Syn model #M092-FD09 stepping motor and the Slo-Syn model #STM1800 stepping motor controller are used to control the opening and closing of the solar air vane and the ambient temperature air vane. The stepping motor can be controlled in incremental 1.8° steps throughout its revolution, giving 200 steps per revolution. The motor has a maximum torque of 450 oz-inch and a maximum speed of 1,000 steps/second. The stepping motor controller contains all the electronics necessary to drive the stepping motor windings and requires only a direction and step pulse from the microprocessor. The direction input is a TTL level from the microprocessor to control clockwise or counterclockwise movement of the armature. The step input requires a TTL level pulse, with each pulse corresponding to a 1.8° movement of the motor. The motor and motor controller will maintain torque to hold the present position of the motor between control pulses from the microprocessor.

IV. THE CONTROL ALGORITHM

The microprocessor uses a combination of both a feed-forward control algorithm and a feed-back control algorithm. The feed-forward algorithm offers the advantage of very rapid response to sudden input changes with no stability problems. The feed-back scheme offers the advantage of high accuracy and adaptation to changes in system parameters. Because the microprocessor is an intelligent controller, it can be programmed to take advantage of both types of control schemes, using the feed-forward scheme for rapid changes, and then switching to the feed-back scheme for maintaining a precise drying temperature.

The feed-forward control scheme looks at the solar air temperature and the ambient air temperature and calculates the position of the motor control on the valves, based on the model of the mixing system discussed in Section II. This model was developed by assuming a simple cosine relationship between valve angle and resistance to airflow in the air inputs as shown in equation (10), section II.

$$R_{\phi} = R_0 \pi r^2 \cos \phi \qquad R_{\theta} = R_0 \pi r^2 \cos \theta \qquad (1)$$

Using the results given for the analogous electric circuit (equation (9), section II), and replacing the currents i_a , i_s , and i_d with the corresponding volume flow rates \dot{v}_a , \dot{v}_s , and \dot{v}_d ,

we have

$$\dot{v}_a = \dot{v}_d \left(\frac{R_s + R_\theta}{R_a + R_\phi + R_s + R_\theta} \right) \quad (2)$$

$$\dot{v}_s = \dot{v}_d \left(\frac{R_a + R_\phi}{R_a + R_\phi + R_s + R_\theta} \right) \quad (3)$$

where

\dot{v}_a = volume rate of flow for ambient air

\dot{v}_s = volume rate of flow for solar-heated air

\dot{v}_d = total volume rate of flow in drying chamber

R_ϕ = resistance offered by ambient air valve (open to angle ϕ)

R_a = other resistance within ambient air path

R_θ = resistance offered by solar air valve (open to angle θ)

R_s = other resistance within solar air path

Because the laboratory prototype uses an electric heating coil, occupying negligible space in the duct pipe, to simulate the solar-heated air, the following assumption is also appropriate:

$$R_a = R_s = 0 \quad (4)$$

Also, the ambient air valve and the solar valve are operated simultaneously by the single stepping motor so that we have

$$\phi = 90^\circ - \theta \quad (5)$$

Using equations (1), (4), and (5) in equations (2) and (3), we

obtain

$$\dot{v}_a = \dot{v}_d \left(\frac{\cos \theta}{\sin \theta + \cos \theta} \right) \quad (6)$$

$$\dot{v}_s = \dot{v}_d \left(\frac{\sin \theta}{\sin \theta + \cos \theta} \right) \quad (7)$$

Experimental verification of equation (6) (for the ambient air volume flow rate) is shown in Figure 4, which indicates a model error of approximately 5% over the operating range. Similar agreement was found in the case of the solar air volume flow rate. The resulting solar valve angle as a function of solar temperature, ambient temperature, and desired dryer temperature is given by

$$\theta_d = \arctan \left(\frac{T_d - T_a}{T_s - T_d} \right) \quad (8)$$

The structure of the control algorithm is as follows:

- 1.) measure T_s and T_a
- 2.) calculate desired valve angle θ_d
- 3.) calculate the desired angle change by subtracting the present angle, θ_p (known from the last iteration of the control algorithm), from the desired angle
- 4.) determine the direction level to the stepping motor controller by the sign (\pm) of $\theta_d - \theta_p$
- 5.) determine the number of steps to be sent to the stepping

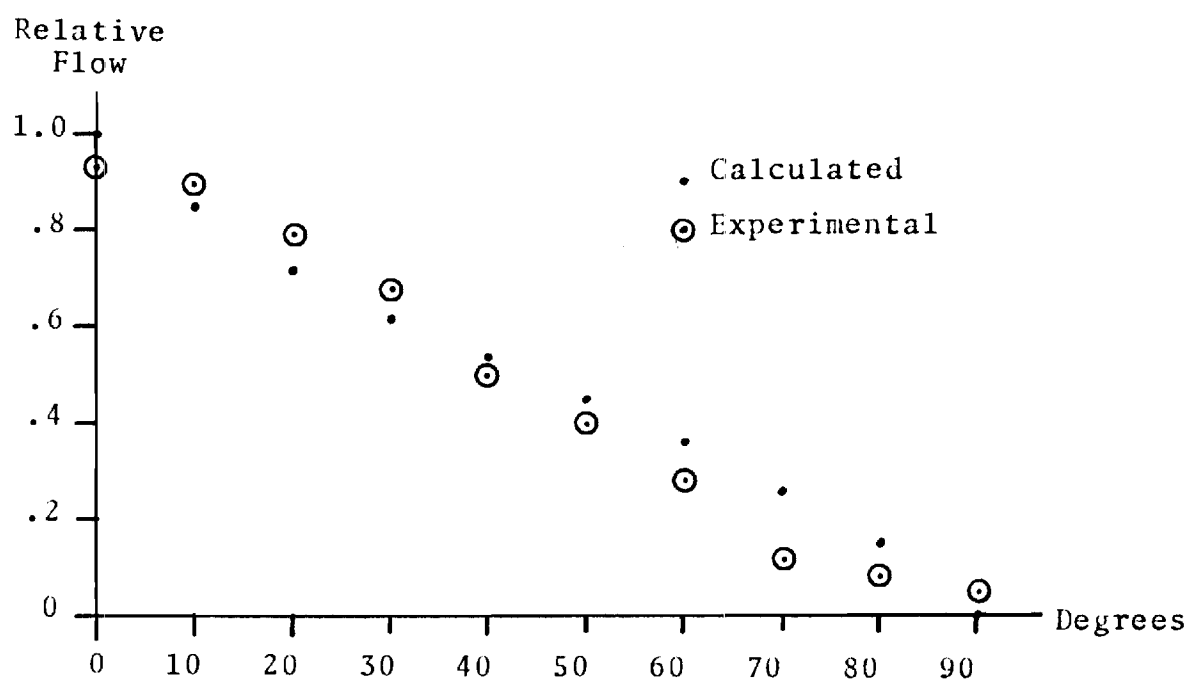


FIGURE 4. Experimental vs. Calculated Air Flow

motor by the magnitude of the difference between θ_d and θ_p . One step would be sent for every 1.8° difference.

After the algorithm has opened the valve to the projected angle, θ_d , the microprocessor will switch over to the feed-back control scheme for final adjustment of valve angle.

The feed-back control scheme monitors the dryer temperature, T_d , and compares the measured value with the desired temperature value and increases or decreases the valve angle to increase or decrease T_d . This feed-back loop has ten seconds of delay to eliminate the problem of rapid changes in valve position due to feed-back instability. The microprocessor stays in the feed-back algorithm until a sudden change is detected in T_s , which indicates that a more rapid correction is required. The algorithm then reverts back to the feed-forward control scheme.

A third algorithm is used to control the action of a backup methane or propane heater. In this algorithm, T_s is constantly monitored to see if it is below the lower limit of the desired dryer temperature. When T_s falls below the lower limit of the dryer temperature, the gas burner is turned on and the system reverts to a burner algorithm, which simply turns on and off a gas burner to maintain the desired dryer temperature.

V. SOFTWARE

The software program controller is written in PLM/80, which is a high level language which generates the 8080 machine code. Since the 80/20 single board computer is not large enough to run a PLM compiler, the programming is done on an MDS 230 system and the programs are transferred to the 80/20 for execution. Use of the MDS development system and the PLM compiler greatly increases the programming efficiency as well as producing well-documented programs that are easy to understand and modify.

The program flowchart shown in Figure 5 contains three main branches depending on whether the solar air temperature is greater than, less than, or equal to the desired dryer temperature range. If the solar temperature is within the desired dryer temperature range, the right hand loop is used and the program opens the solar valve full and uses the solar air directly for drying.

If the solar air drops below the desired dryer range, the program switches to the left loop which controls the action of the backup burner by turning it on and off to maintain a desired temperature for the dryer. This loop also checks the solar temperature to determine whether it has risen enough to switch back from the backup burner to solar drying.

If the solar temperature gets above the desired drying range, then the middle loop is entered which mixes the solar air with ambient air to achieve a lower desired drying temperature. This

T_s = Solar Temperature
 T_a = Ambient Temperature
 T_d = Dryer Temperature
 U = Upper Dryer Limit
 L = Lower Dryer Limit
 $H = L + \frac{U-L}{2}$

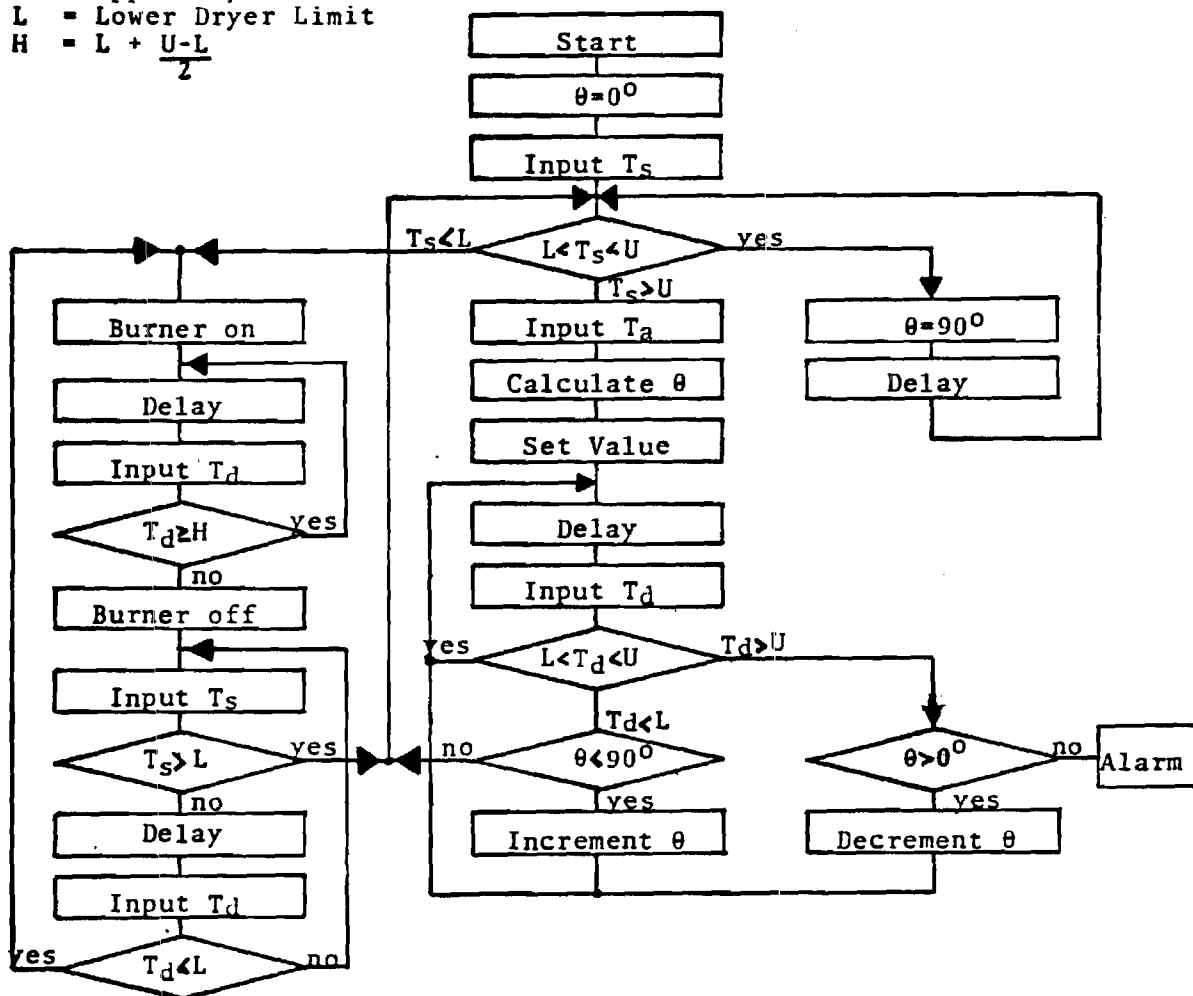


FIGURE 5. Controller Flow Chart

is accomplished by first going through a feed-forward control algorithm where T_s , T_d , and T_a are used to calculate the proper opening for the mixing valves. Once this initial valve opening is achieved, the program reverts to a slower acting feed-back loop to increment or decrement the valve opening to achieve an accurate desired temperature.

VI. EXPERIMENTAL PROCEDURE

To test the operation of the microprocessor controller, an experimental air mixer was constructed using an eight inch axial blower fan and standard eight inch furnace duct. The air mixing valves were constructed by means of a circular louver which rotates inside the duct pipe.

One valve was mounted in the solar air duct and the second valve in the ambient air duct with a chain drive between the valves so that as one valve is opened, the other is closed. An angle of $\theta = 0^{\circ}$ represents the solar air being totally shut off and the ambient air being totally open, whereas an angle of $\theta = 90^{\circ}$ indicates the solar air valve totally open and the ambient air valve totally closed.

The backup gas heater was constructed from parts of a standard home gas heater system plus a Robertshaw model #VX700 electronic starter system for automatic pilot re-lighting. This system uses a high voltage spark to ignite a pilot light, and the pilot light is then used to light the main burner.

A three phase 3,000 watt electric heater was constructed using heating coils mounted in a section of eight inch duct pipe to simulate the solar air that would normally be available from a standard solar collector. A three phase Variac was used to vary the amount of heat available in the simulated solar collector. By varying the upper and lower desired dryer temperature limits and by changing the amount of power

delivered to the solar air simulator, all of the software loops of the controller were checked for proper operation.

Figure 6 shows a plot of solar temperature, T_s , dryer temperature, T_d , and solar louver angle θ as functions of time in a typical test of the feed-back control loop section of the controller program. (During the start-up portion of the graph, the system was initialized using the feed-forward control.) When the dryer temperatures were below the lower desired limit, the controller increased the angle θ to allow more solar heated air. Likewise, when the dryer exceeded the upper desired limit, the controller would decrease the valve angle, reduce the amount of solar heated air, and increase the amount of ambient air. While the system was in the burner control loop of the program, readings were taken of dryer temperature T_d and state of the burner (on-off). This relationship is shown in Figure 7. When T_d exceeds the desired range, the burner turns off; when T_d is below the desired range, the burner is activated. As the graph shows, T_d is not so smoothly level as in Figure 6. This results from the simple two-state configuration of the burner, by contrast with the continuous range of settings of the solar and ambient air valves. Also included is a graph (Figure 8) of the burner temperature response as a function of elapsed time.

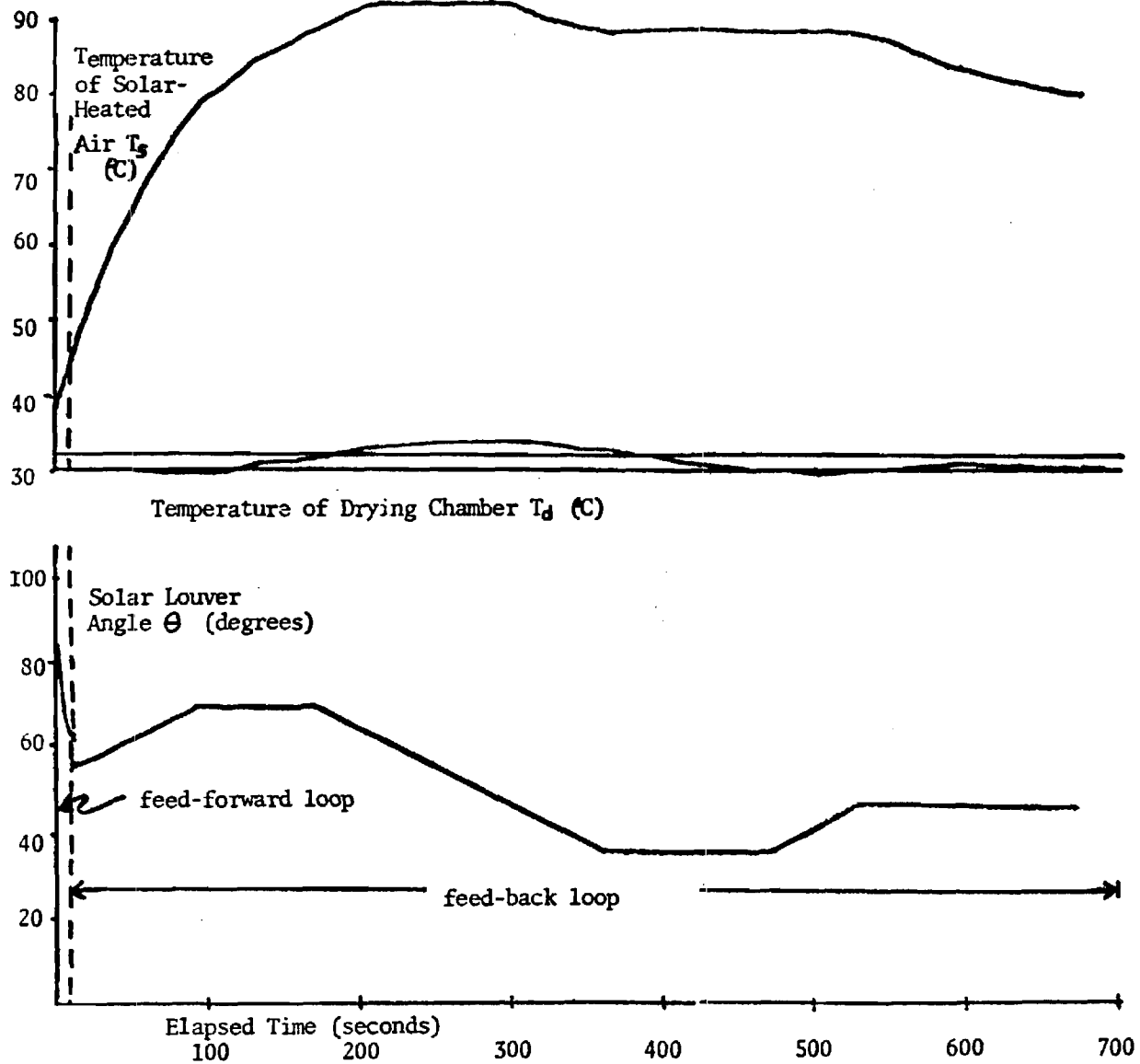


FIGURE 6. T_s , T_d , and θ as Functions of Time During a Test of the Controller Program

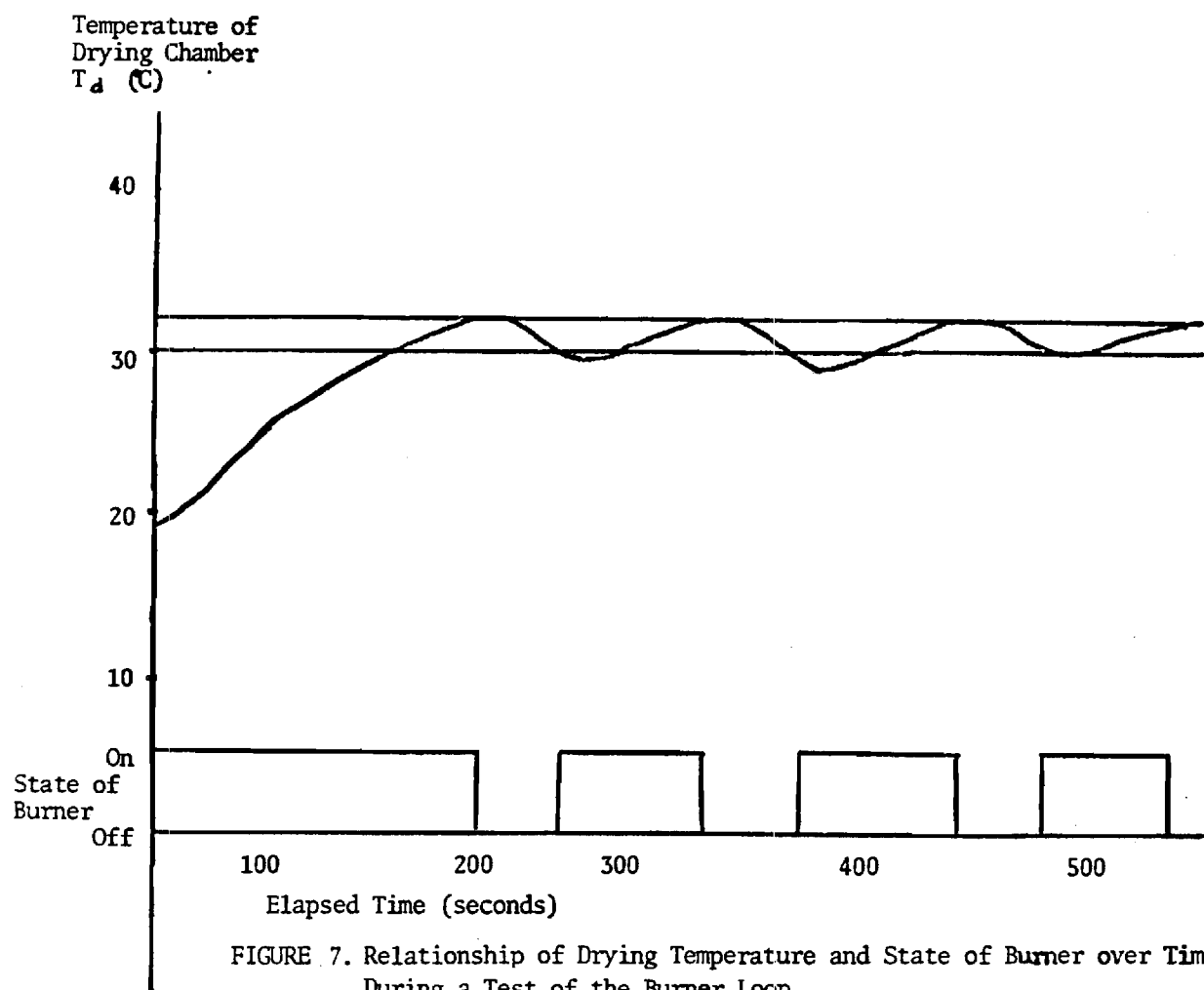


FIGURE 7. Relationship of Drying Temperature and State of Burner over Time During a Test of the Burner Loop

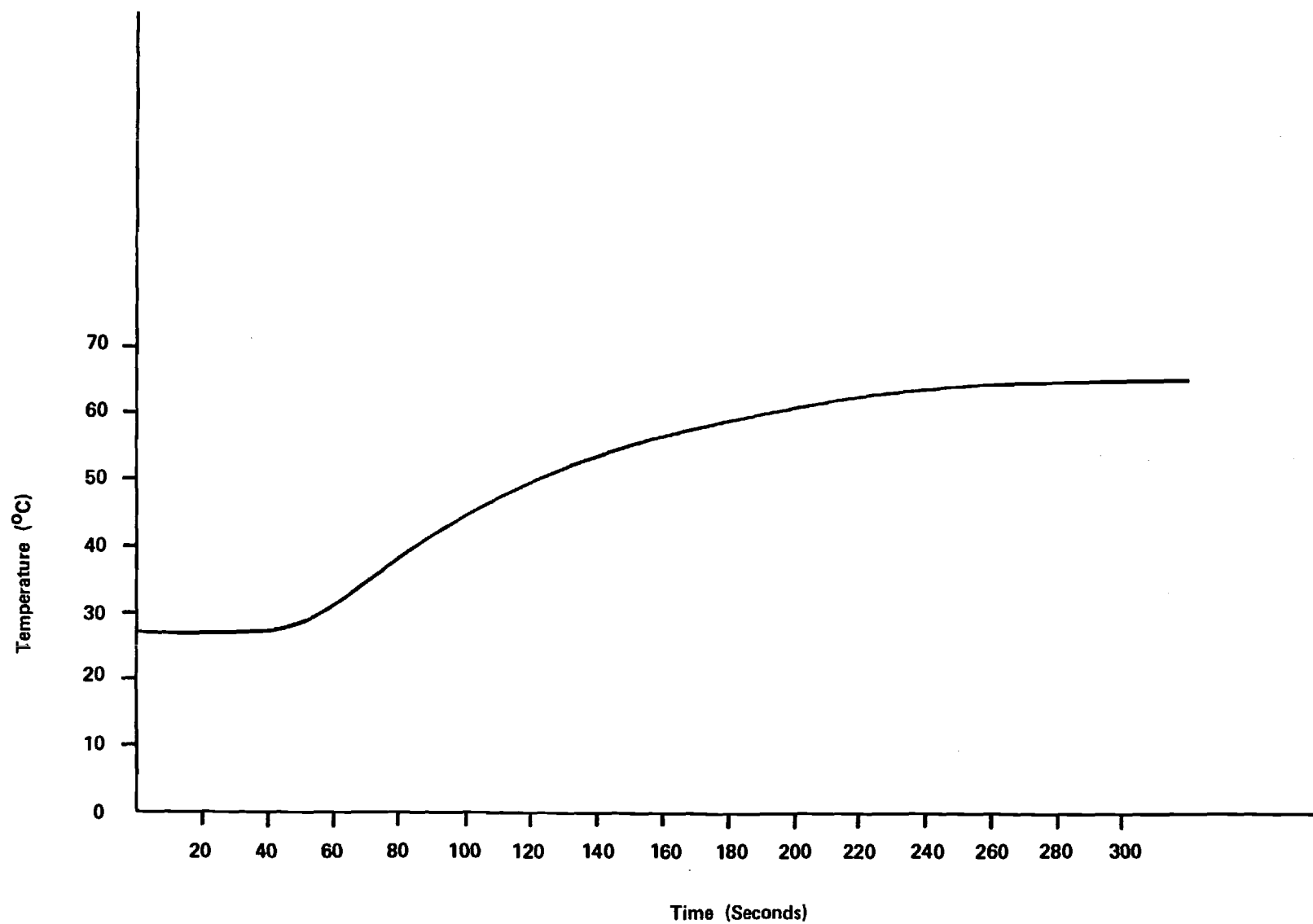


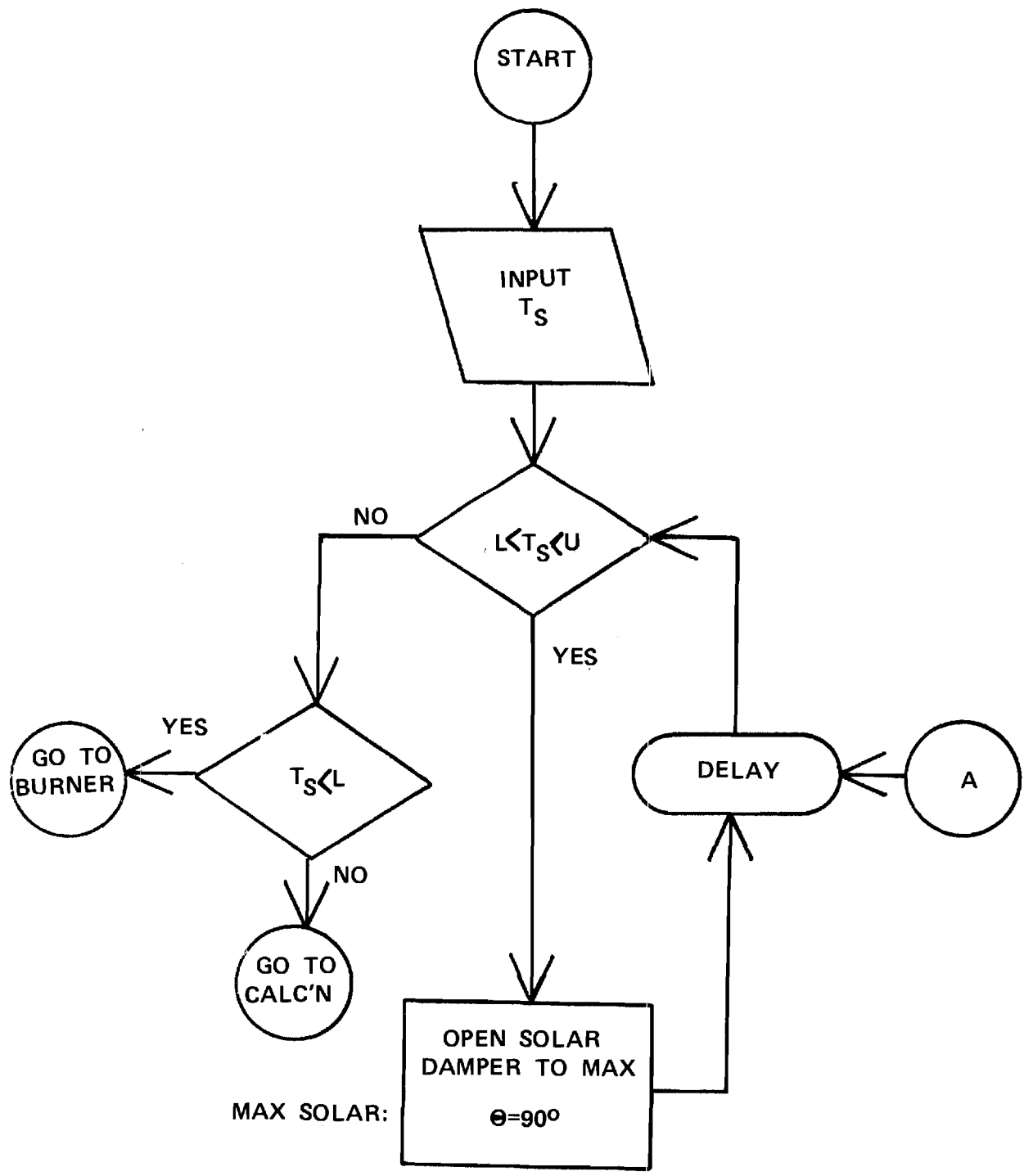
Figure 8. Temperature of Burner-Heated Air vs. Time from Switch-On.

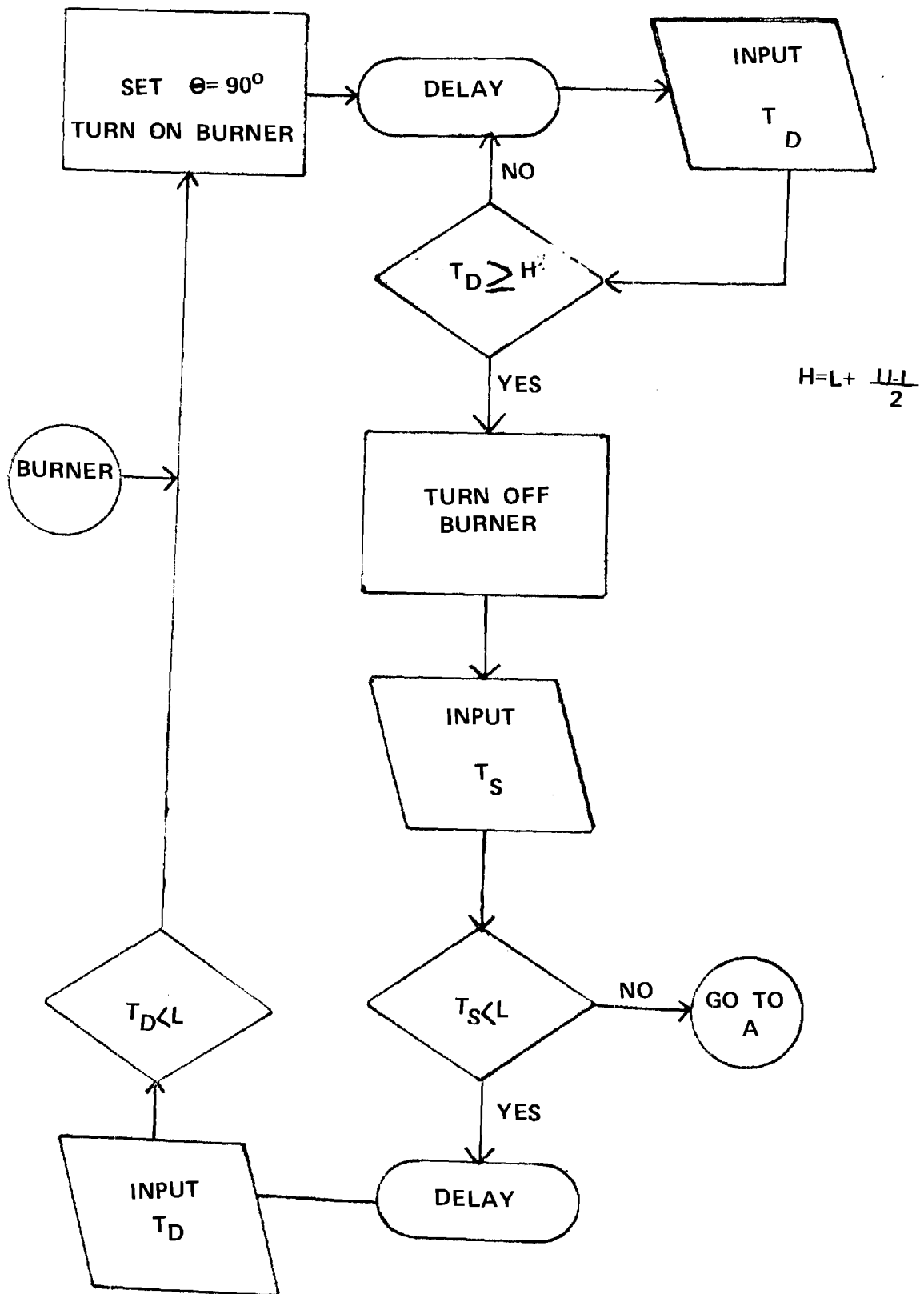
VII. RESULTS AND CONCLUSIONS

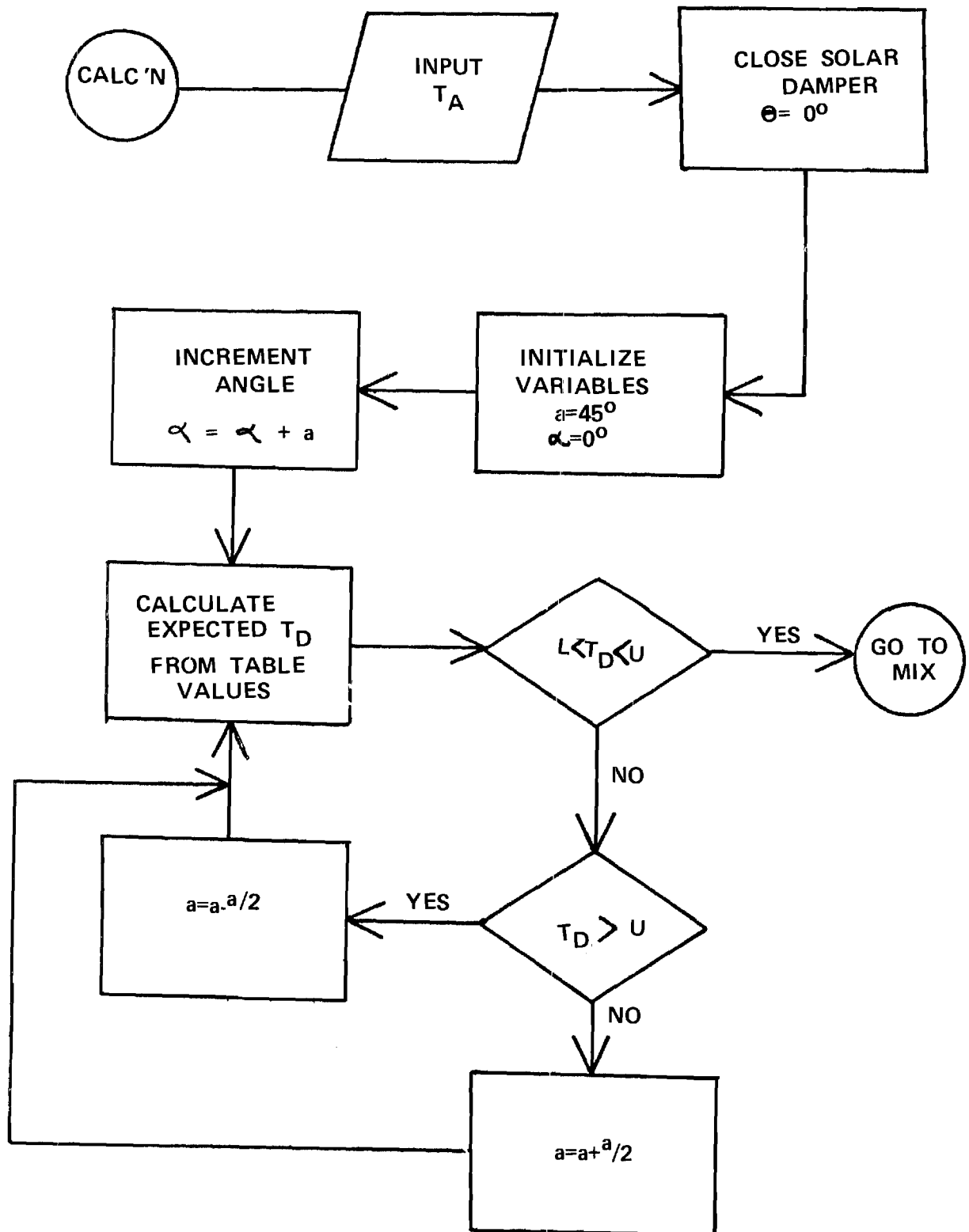
The results of this research indicate that the micro-processor system described is capable of controlling a typical drying process. Since the laboratory equipment cost was less than \$2,000, a cost effective system should be feasible on an industrial scale. One of the most important features of the microprocessor system is the ability of the system to expand with little increase in system cost. This feature will permit additional energy conservation algorithms to be incorporated to increase the system cost effectiveness. Additional control functions such as graduated heater control could also be added with little additional cost.

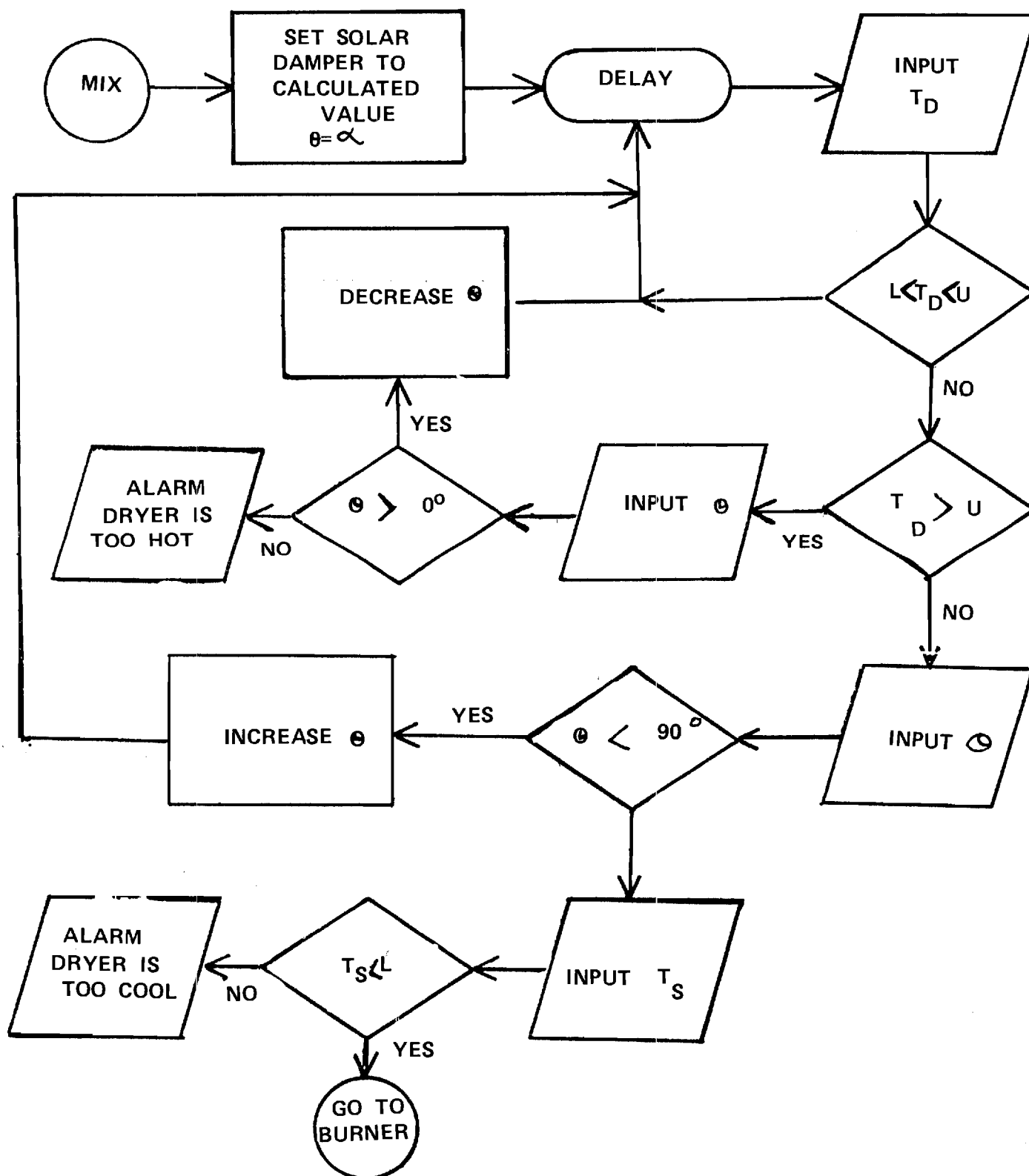
APPENDIX A

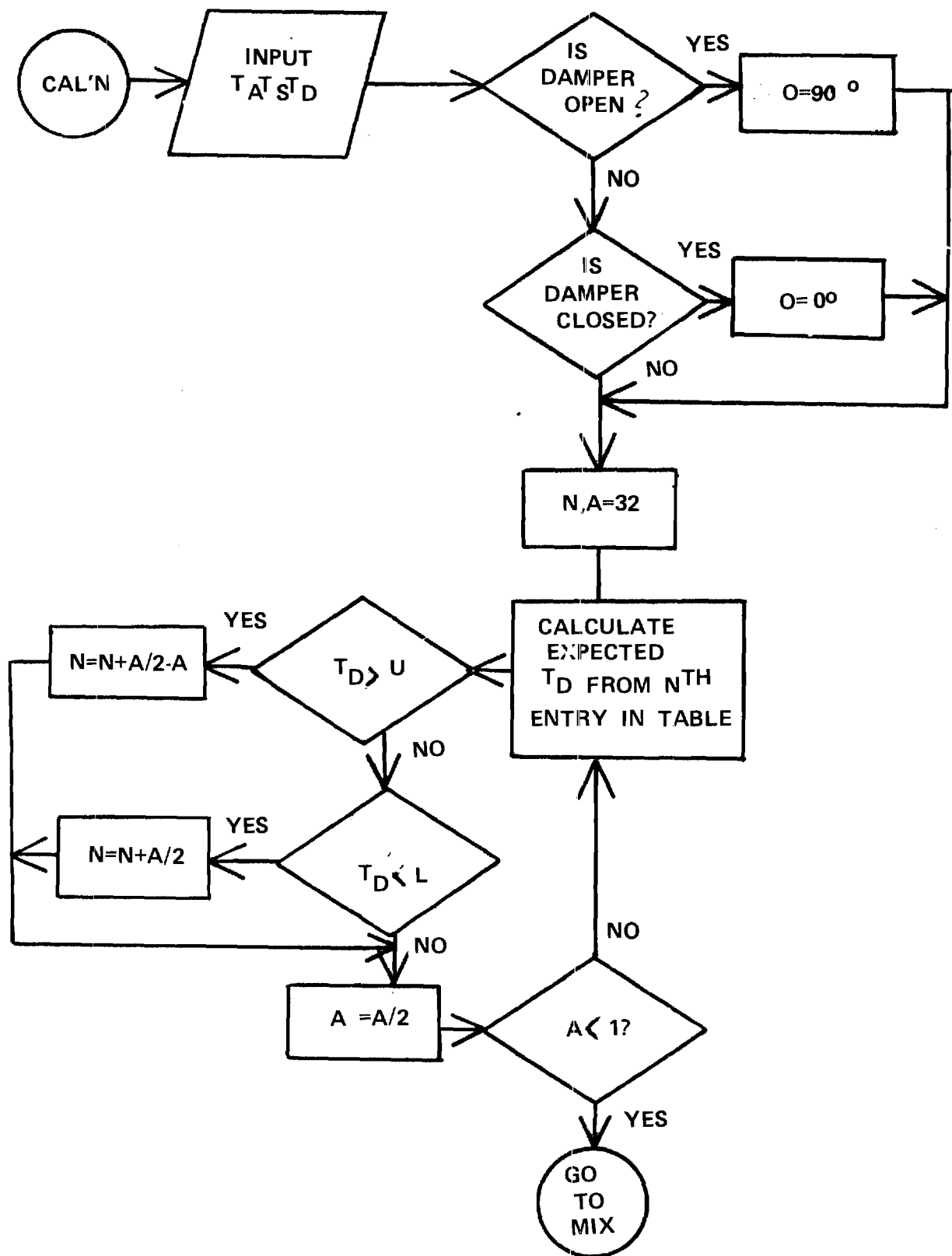
DETAILED FLOWCHARTS
FOR CONTROLLING DAMPERS AND BURNERS











APPENDIX B

PROGRAM LISTING

ISIS-II PL/M-80 V3.0 COMPILATION OF MODULE USDA
 OBJECT MODULE PLACED IN :F1:USDA.OBJ
 COMPILER INVOKED BY: PLM80 :F1:USDA.SRC

```

1          USDA:DO;          /*DATE:21 MAY 80*/

                        /*SOLAR---LPN=1*/
                        /*BURNER---LPN=2*/
                        /*LOOP----LPN=3*/
                        /*MIX-----LPN=4*/
                        /*MAINT---LPN=5*/

2      1      DECLARE OE4 BYTE INITIAL(0FFH);
3      1      DECLARE (I,U) ADDRESS DATA(300,320);
4      1      DECLARE (THETA,N,LPN,TS,TA,TD) ADDRESS;
5      1      DECLARE (ALT,J,I,A) BYTE INITIAL(1,0,0,0);
6      1      DECLARE KS(50) ADDRESS DATA(3282,1689,1157,891,731,624,547,
                        489,444,408,378,353,331,313,296,282,269,258,247,238,
                        229,221,213,206,200,194,188,183,178,173,168,163,159,
                        155,151,143,140,136,132,129,126,122,119,116,113,109,
                        106,103,100);
7      1      DECLARE KA(50) ADDRESS DATA(100,103,106,109,113,116,119,122,
                        126,129,132,136,140,143,147,151,155,159,163,168,173,
                        178,183,188,194,200,206,213,221,229,238,247,258,269,
                        282,296,313,331,353,378,408,444,489,547,634,731,892,
                        1157,1689,3282);

8      1      CC:PROCEDURE(CHAR) EXTERNAL;
9      2      DECLARE CHAR BYTE;
10     2      END CC;

11     1      NMOUT:PROCEDURE(ASCII) EXTERNAL;
12     2      DECLARE ASCII BYTE;
13     2      END NMOUT;

14     1      TMP:PROCEDURE;
15     2      CALL CC('L');
16     2      CALL CO('P');
17     2      CALL CO('N');
18     2      CALL CO(' ');
19     2      CALL NMOUT(LOW(LPN));

20     2      OE4=(0F8H AND OE4) OR 5;
21     2      OUTPUT(0E4H)=OE4;          /*SELECT SOLAR*/
22     2      OUTPUT(0EAH)=1;
23     2      OUTPUT(0EAH)=0;          /*PULSE TO INIT CONV*/
24     2      CALL CO(' ');
25     2      CALL CO(' ');
26     2      CALL CO('T');
27     2      CALL CO('S');
28     2      CALL CO('=');
29     2      CALL TIME(100);
30     2      TS=(0C0H AND INPUT(0EAH))*4+(NOT INPUT(0E8H));
31     2      CALL NMOUT(HIGH(TS));

```

```

32      2      CALL NMOUT(LOW(TS));

33      2      OE4=OE4 OR 7;
34      2      OUTPUT(0E4H)=OE4;          /*SELECT AMB TMP*/
35      2      OUTPUT(0E4H)=1;
36      2      OUTPUT(0E4H)=0;
37      2      CALL CO(' ');
38      2      CALL CO(' ');
39      2      CALL CO('T');
40      2      CALL CO('A');
41      2      CALL CO('=');
42      2      CALL TIME(100);
43      2      TA=(0C0H AND INPUT(0E4H))*4+(NOT INPUT(0E8H));
44      2      CALL NMOUT(HIGH(TA));
45      2      CALL NMOUT(LOW(TA));

46      2      OE4=(0F8H AND OE4) OR 6;    /*SELECT DRYER TMP*/
47      2      OUTPUT(0E4H)=OE4;
48      2      OUTPUT(0E4H)=1;
49      2      OUTPUT(0E4H)=0;
50      2      CALL CO(' ');
51      2      CALL CO(' ');
52      2      CALL CO('T');
53      2      CALL CO('D');
54      2      CALL CO('=');
55      2      CALL TIME(100);
56      2      TD=(0C0H AND INPUT(0E4H))*4+(NOT INPUT(0F8H));
57      2      CALL NMOUT(HIGH(TD));
58      2      CALL NMOUT(LOW(TD));

59      2      CALL CO(' ');
60      2      CALL CO(' ');
61      2      CALL CO('T');
62      2      CALL CO('H');
63      2      CALL CO('F');
64      2      CALL CO('T');
65      2      CALL CO('A');
66      2      CALL CO('=');
67      2      CALL NMOUT(LOW(THETA));
68      2      CALL CO(0DH);
69      2      CALL CO(0AH);
70      2      END TMP;

71      1      FWD:PROCEDURE; /*PULSES THE MOTOR CONTROL THAT
                          OPENS THE SOLAR DAMPER(1.8DEG/PULSE)*/

72      2      OE4=OE4 AND 0EFH; /*SET BIT 4--PORT E4
                          HAS INVERTED OUTPUTS*/
73      2      OUTPUT(0E4H)=OE4;
74      2      DO I=1 TO 5;
75      3      CALL TIME(100); /*10 MS DELAY*/
76      3      END;
77      2      OE4=OE4 OR 10H; /*ZERO BIT 4*/
78      2      OUTPUT(0E4H)=OE4;
79      2      DO I=1 TO 5;
80      3      CALL TIME(100);

```

```

81      3      END;
82      2      END FWD;

83      1      DELAY:PROCEDURE;
84      2          DO I=1 TO 4;
85      3          DO J=1 TO 250;          /*10 SEC DELAY*/
86      4          CALL TIME(100);
87      4          END;
88      3          END;
89      2      END DELAY;

/*THE FOLLOWING PROCEDURE OPENS SOLAR DAMPER TO MAX POSITION(90DEG
DEG90:PROCEDURE;
90      1          DO WHILE(SHR(INPUT(0E6H),1));
91      2              CALL FWD;
92      3          END;
93      3          THETA=50;
94      2      END DEG90;

96      1      BKWD:PROCEDURE;          /*PULSES MOTOR CONTROL TO
          CLOSE SOLAR DAMPER(1.8DEG/PULSE)*/

97      2          OE4=OE4 AND 0F7H;          /*SET BIT 3*/
98      2          OUTPUT(0E4H)=OE4;          /*RAISE CONTROL LINE
          FOR BWK(CW) PULSES*/

99      2          DO I=1 TO 5;
100     3          CALL TIME(100);          /*10 MS DELAY*/
101     3          END;
102     2          OE4=OE4 OR 8H;          /*ZERO BIT 3*/
103     2          OUTPUT(0E4H)=OE4;          /*LOWER CONTROL LINE*/
104     2          DO I=1 TO 5;
105     3          CALL TIME(100);
106     3          END;
107     2      END BKWD;

108     1      INIT:OE4=0FFH;          /*INITIALIZE CONTROL WORD
          FOR PORT E4*/

109     1          OUTPUT(0EBH)=98H;
110     1          OUTPUT(0E7H)=89H;

111     1      START:DO WHILE (INPUT(0E6H));          /*CLOSE DAMPER TO SOLAR AIR*/
112     2          CALL BKWD;
113     2          END;
114     1          THETA=0;

115     1      SCLAR:LPN=1;
116     1          CALL CO(0AH);
117     1          CALL CO(0DH);
118     1          CALL CO('S');
119     1          CALL CO('O');
120     1          CALL CO('L');
121     1          CALL CO('A');
122     1          CALL CO('R');
123     1          CALL CO(0DH);

```

```

124 1      CALL CO(0AH);
125 1      CALL TMP;
126 1      IF(TS>U)THEN GOTO MIX;
128 1      CALL DEG90;      /*TS<U,SOLAR AIR MAX*/
129 1      IF(TS<L)THEN GOTO BURNER;
131 1      ELSE CALL DELAY;      /*ELSE L<TS<U;SO STAY
                                IN SOLAR ROUTINE*/
132 1      GOTO SOLAR;

133 1      BURNER: LPN=2;
134 1      OUTPUT(0E4H)=(0E4 AND 0DFH);      /*LIGHT BURNER*/
135 1      INTCON: CALL CO('B');
136 1      CALL CO('U');
137 1      CALL CO('R');
138 1      CALL CO('N');
139 1      CALL CO('E');
140 1      CALL CO('R');
141 1      CALL CO(0DH);
142 1      CALL CO(0AH);
143 1      CALL TMP;

144 1      IF (TD<L+(U-L)/2) THEN CALL DELAY;
146 1      ELSE GO TO BRNOFF;
147 1      GO TO INTCON;
148 1      BRNOFF: 0E4=0E4 OR 20H;      /*ZERO BIT 5 OF PORT1*/
149 1      OUTPUT(0E4H)=0E4;      /*TURN OFF BURNER*/

150 1      LOOP:LPN=3;
151 1      CALL CO('L');
152 1      CALL CO('O');
153 1      CALL CO('O');
154 1      CALL CO('P');
155 1      CALL CO(0AH);
156 1      CALL CO(0DH);
157 1      CALL TMP;
158 1      IF (TS<L)THEN CALL DELAY;
160 1      ELSE GOTO SOLAR;
161 1      CALL TMP;
162 1      IF(TD<L)THEN GOTO BURNER; /*IF TD<L & TS<L*/
164 1      ELSE GOTO LOOP; /*IF TD>L & TS<L*/

165 1      MIX:LPN=4;

166 1      CALL CO('M');
167 1      CALL CO('I');
168 1      CALL CO('X');
169 1      CALL CO(0AH);
170 1      CALL CO(0DH);
171 1      CALL TMP;

/*CHECK DAMPER POSITION; IF FULLY OPFN, THETA=50*/

172 1      IF((INPUT(0E6H) AND 1)=0)THEN THETA=0;
174 1      IF((INPUT(0E6H) AND 2)=0)THEN THETA=50;

/*ITERATIVE PROCEDURE FOR DETERMINING

```

THEORETICAL SETTING ,GIVEN TS & TA*/

```

176 1      N,A=32;
177 1      CALL CO('I');
178 1      CALL CO('T');
179 1      CALL CO('E');
180 1      CALL CO('R');
181 1      CALL CO(0DH);
182 1      CALL CO(0AH);
183 1      ITER: DO I=0 TO 5;
184 2          TD=(TS*10/KS(N)+TA*10/KA(N))*10;
185 2          A=SHR(A,1);
186 2          IF(TD>U)THEN N=N-SHL(A,1)+A;
188 2          IF(TD<L)THEN N=N+A;
190 2          CALL CO(' ');
191 2          CALL CO('N');
192 2          CALL CO('=');
193 2          CALL NMOUT(LOW(N));
194 2          CALL CO(0DH);
195 2          CALL CO(0AH);
196 2          IF(N>49)THEN N=48;
198 2          END;
199 1          DO WHILE (N<THETA);
200 2              CALL BKWD;
201 2              THETA=THETA-1;
202 2              END;
203 1          DO WHILE(N>THETA);
204 2              CALL FWD;
205 2              THETA=THETA+1;
206 2              END;

207 1          CALL CO('T');
208 1          CALL CO('H');
209 1          CALL CO('E');
210 1          CALL CO('T');
211 1          CALL CO('A');
212 1          CALL CO('=');
213 1          CALL NMOUT(LOW(THETA));
214 1          CALL CO(0DH);
215 1          CALL CO(0AH);

```

/*THIS ROUTINE WILL MAINTAIN THE CORRECT DAMPER SETTING
FOR THE DESIRED DRYER TEMPERATURE*/

```

216 1      MAINT: OE4=(OE4 AND 0F8H) OR 6;
217 1      OUTPUT(0E4H)=OE4;          /*SELECT TD*/
218 1      OUTPUT(0EAH)=1;
219 1      OUTPUT(0EAH)=0;
220 1      CALL CO('M');
221 1      CALL CO('A');
222 1      CALL CO('I');
223 1      CALL CO('N');
224 1      CALL CO('T');
225 1      CALL CO(0AH);
226 1      CALL CO(0DH);
227 1      CALL DELAY;          /*10 SEC DELAY*/

```

```

228 1          CALL TMP;

/*THE FOLLOWING ROUTINES COMPENSATE FOR ANY POSSIBLE INACCURACIES
  IN THE THEORETICAL CALCULATION FOR THE DAMPER SETTING*/

229 1          ICR:   IF((TD>U) AND (THETA>0)) THEN DO;
231 2                      THETA=THETA-1;
232 2                      CALL FWD;
233 2                      END;
234 1          INCR:  IF((TD<L) AND (THETA<50)) THEN DO;
236 2                      CALL FWD;
237 2                      THETA=THETA+1;
238 2                      END;
239 1          CALL TMP;

/*THIS ROUTINE WILL MAINTAIN DESIRED DRYER TEMP INDEFINITELY
  UNLESS SOLAR TEMP DROPS BELOW LOWER LIMIT;
  IN WHICH CASE, PROGRAM RETURNS TO SOLAR ROUTINE*/

240 1          IF(TS<=L)THEN GOTO SOLAR;

/*IF THE DRYER COMPARTMENT BECCMES TOO HOT OR TO COOL,
  AND THE DAMPER IS AT MIN OR MAX SETTING RESPECTIVELY,
  AN ALARM LIGHT WILL BE ACTIVATED AND THE PROGRAM HALTED*/

242 1          IF((TD>U) AND (THETA=0))THEN GO TO ALARM;
244 1          IF((TD<L) AND (THETA=50))THEN GOTO ALARM;

246 1          GO TO MAINT;

247 1          ALARM:  OE4=OE4 AND 0BFH;    /*SET ALARM BIT*/
248 1          OUTPUT(0E4H)=OE4;    /*RAISE ALARM LINE*/
249 1          END USDA;

```

MODULE INFORMATION:

```

CODE AREA SIZE      = 06A4H    1700D
VARIABLE AREA SIZE  = 0011H    17D
MAXIMUM STACK SIZE  = 0006H    6D
312 LINES READ
0 PROGRAM ERROR(S)

```

END OF PL/M-80 COMPIIATION

ISIS-II PL/M-80 V3.0 COMPILATION OF MODULE USDA
 OBJECT MODULE PLACED IN :F1:USDA.OBJ
 COMPILER INVOKED BY: PLM80 :F1:USDA.SRC CODE

```

1          USDA:DC;          /*DATE:21 MAY 80*/

          /*SOLAR---LPN=1*/
          /*BURNER---LPN=2*/
          /*LOCP----LPN=3*/
          /*MIX-----LPN=4*/
          /*MAINT---LPN=5*/

2  1      DECLARE OE4 BYTE INITIAL(0FFH);
3  1      DECLARE (L,U) ADDRESS DATA(300,320);
4  1      DECLARE (THFTA,N,LPN,TS,TA,TD) ADDRESS;
5  1      DECLARE (ALT,J,I,A) BYTE INITIAL(1,0,0,0);
6  1      DECLARE KS(50) ADDRESS DATA(3282,1689,1157,891,731,624,547,
          489,444,408,378,353,331,313,296,282,269,258,247,238,
          229,221,213,206,200,194,188,183,178,173,168,163,159,
          155,151,143,140,136,132,129,126,122,119,116,113,109,
          106,103,100);
7  1      DECLARE KA(50) ADDRESS DATA(100,103,106,109,113,116,119,122,
          126,129,132,136,140,143,147,151,155,159,163,168,173,
          178,183,188,194,200,206,213,221,229,238,247,258,269,
          282,296,313,331,353,378,408,444,489,547,634,731,892,
          1157,1689,3282);

8  1      CC:PROCEDURE(CHAR) EXTERNAL;
9  2      DECLARE CHAR BYTE;
10 2      END CC;

11 1      NMOUT:PROCEDURE(ASCII) EXTERNAL;
12 2      DECLARE ASCII BYTE;
13 2      END NMOUT;

14 1      TMP:PROCEDURE;

          ; STATEMENT # 14
          ; PROC TMP
15 2      CALL CO('L');

          ; STATEMENT # 15
          0479 0E4C MVI C,4CH
          047B CD0000 CALL CO
16 2      CALL CO('P');

          ; STATEMENT # 16
          047E 0E50 MVI C,50H
          0480 CD0000 CALL CO
17 2      CALL CO('N');

          ; STATEMENT # 17
          0483 0E4E MVI C,4EH
          0485 CD0000 CALL CO
18 2      CALL CO(' ');

          ; STATEMENT # 18
          0488 0E20 MVI C,20H
          048A CD0000 CALL CO

```

```

19      2      CALL NMOUT(LOW(LPN));                ; STATEMENT # 19
          048D 2A0500      LHLD    LPN
          0490 7D          MOV     A,L
          0491 4F          MOV     C,A
          0492 CD0000      CALL    NMOUT

20      2      CE4=(0F8H AND 0E4) OR 5;            ; STATEMENT # 20
          0495 3A0000      LDA     0E4
          0498 E6F8      ANI     0F8H
          049A F605      ORI     5H
          049C 320000      STA     0E4

21      2      OUTPUT(0E4H)=0E4;                  /*SELECT SOLAR*/
                                                  ; STATEMENT # 21
          049F D3E4      OUT     0E4H

22      2      OUTPUT(0EAH)=1;                    ; STATEMENT # 22
          04A1 3E01      MVI     A,1H
          04A3 D3EA      OUT     0EAH

23      2      OUTPUT(0EAH)=0;                    /*PULSE TO INIT CONV*/
                                                  ; STATEMENT # 23
          04A5 3E00      MVI     A,0H
          04A7 D3EA      OUT     0EAH

24      2      CALL CO(' ');                      ; STATEMENT # 24
          04A9 0E20      MVI     C,20H
          04AB CD0000      CALL    CO

25      2      CALL CO(' ');                      ; STATEMENT # 25
          04AE 0E20      MVI     C,20H
          04B0 CD0000      CALL    CO

26      2      CALL CO('T');                      ; STATEMENT # 26
          04B3 0E54      MVI     C,54H
          04B5 CD0000      CALL    CO

27      2      CALL CO('S');                      ; STATEMENT # 27
          04B8 0E53      MVI     C,53H
          04BA CD0000      CALL    CO

28      2      CALL CO('=');                      ; STATEMENT # 28
          04BD 0E3D      MVI     C,3DH
          04BF CD0000      CALL    CO

29      2      CALL TIME(100);                    ; STATEMENT # 29
          04C2 3E64      MVI     A,64H
          04C4 CD0000      CALL    0P0105

30      2      TS=(0C0H AND INPUT(0EAH))*4+(NOT INPUT(0F8H));
                                                  ; STATEMENT # 30
          04C7 DBEA      IN      0EAH
          04C9 E6C0      ANI     0C0H
          04CB 6F      MOV     L,A
          04CC 2600      MVI     H,0
          04CE 29      DAD     H
          04CF 29      DAD     H
          04D0 DBE8      IN      0E8H

```

		04D2	2F	CMA	
		04D3	5F	MOV	E,A
		04D4	1600	MVI	D,0
		04D6	19	DAD	D
		04D7	220700	SHLD	TS
31	2			CALL NMOUT(HIGH(TS));	
					; STATEMENT # 31
		04DA	2A0700	LHLD	TS
		04DD	7C	MOV	A,H
		04DE	4F	MOV	C,A
		04DF	CD0000	CALL	NMOUT
32	2			CALL NMOUT(LOW(TS));	
					; STATEMENT # 32
		04E2	2A0700	LHLD	TS
		04E5	7D	MOV	A,L
		04E6	4F	MOV	C,A
		04E7	CD0000	CALL	NMOUT
33	2			OE4=OE4 OR 7;	
					; STATEMENT # 33
		04EA	3A0000	LDA	OE4
		04ED	F607	ORI	7H
		04EF	320000	STA	OE4
34	2			OUTPUT(OE4H)=OE4;	
					/*SELECT AMB TMP*/
					; STATEMENT # 34
		04F2	D3EA	OUT	OE4H
35	2			OUTPUT(OE4H)=1;	
					; STATEMENT # 35
		04F4	3E01	MVI	A,1H
		04F6	D3EA	OUT	OE4H
36	2			OUTPUT(OE4H)=0;	
					; STATEMENT # 36
		04F8	3E00	MVI	A,0H
		04FA	D3EA	OUT	OE4H
37	2			CALL CO(' ');	
					; STATEMENT # 37
		04FC	0E20	MVI	C,20H
		04FE	CD0000	CALL	CO
38	2			CALL CO(' ');	
					; STATEMENT # 38
		0501	0E20	MVI	C,22H
		0503	CD0000	CALL	CO
39	2			CALL CO('T');	
					; STATEMENT # 39
		0506	0E54	MVI	C,54H
		0508	CD0000	CALL	CO
40	2			CALL CO('A');	
					; STATEMENT # 40
		050B	0E41	MVI	C,41H
		050D	CD0000	CALL	CO
41	2			CALL CO('=');	
					; STATEMENT # 41
		0510	0E3D	MVI	C,3DH
		0512	CD0000	CALL	CO
42	2			CALL TIME(100);	
					; STATEMENT # 42

```

0515 3E64          MVI    A,64H
0517 CD0000      CALL    GP0105
43   2          TA=(0C0H AND INPUT(0EAH))*4+(NOT INPUT(0F8H));
                                ; STATEMENT # 43
051A DBEA          IN     0EAH
051C E6C0          ANI    0C0H
051E 6F           MOV    L,A
051F 2600          MVI    H,0
0521 29           DAD    H
0522 29           DAD    H
0523 DBE8          IN     0F8H
0525 2F           CMA
0526 5F           MOV    E,A
0527 1600          MVI    L,0
0529 19           DAD    D
052A 220900      SHLD   TA
44   2          CALL NMOUT(HIGH(TA));
                                ; STATEMENT # 44
052D 2A0900      LHLD   TA
0530 7C           MOV    A,H
0531 4F           MOV    C,A
0532 CD0000      CALL    NMOUT
45   2          CALL NMOUT(LOW(TA));
                                ; STATEMENT # 45
0535 2A0900      LHLD   TA
0538 7D           MOV    A,L
0539 4F           MOV    C,A
053A CD0000      CALL    NMOUT
46   2          OE4=(0F8H AND OE4) OR 6;
                                /*SELECT DRYER TMP*/
                                ; STATEMENT # 46
053D 3A0000      LDA     OE4
0540 E6F8          ANI    0F8H
0542 F606          ORI    6H
0544 320000      STA     OE4
47   2          OUTPUT(0E4H)=OE4;
                                ; STATEMENT # 47
0547 D3E4          OUT    0E4H
48   2          OUTPUT(0EAH)=1;
                                ; STATEMENT # 48
0549 3F01          MVI    A,1H
054B D3FA          OUT    0FAH
49   2          OUTPUT(0EAH)=0;
                                ; STATEMENT # 49
054D 3F00          MVI    A,0H
054F D3EA          OUT    0EAH
50   2          CALL CO(' ');
                                ; STATEMENT # 50
0551 0E20          MVI    C,20H
0553 CD0000      CALL    CO
51   2          CALL CO(' ');
                                ; STATEMENT # 51
0556 0E20          MVI    C,20H
0558 CD0000      CALL    CO
52   2          CALL CO('T');
                                ; STATEMENT # 52
055B 0E54          MVI    C,54H

```

```

53  2  055D  CD0000          CALL      CO
          CALL CO('E');
                                     ; STATEMENT # 53

          0560  0F44          MVI      C,44H
          0562  CD0000          CALL      CO
54  2          CALL CO('=');
                                     ; STATEMENT # 54

          0565  0E3D          MVI      C,3DH
          0567  CD0000          CALL      CC
55  2          CALL TIME(100);
                                     ; STATEMENT # 55

          056A  3E64          MVI      A,64H
          056C  CD0000          CALL      @P0105
56  2          TD=(0C0H AND INPUT(0EAH))*4+(NOT INPUT(0E8H));
                                     ; STATEMENT # 56

          056F  DBEA          IN        0EAH
          0571  E6C0          ANI      0C0H
          0573  6F           MOV      L,A
          0574  2620          MVI      H,0
          0576  29           DAD      H
          0577  29           DAD      H
          0578  DBE8          IN        0E8H
          057A  2F           CMA
          057B  5F           MOV      E,A
          057C  1600          MVI      D,0
          057E  19           DAD      E
          057F  220B00        SHLD     TD
57  2          CALL NMOUT(HIGH(TD));
                                     ; STATEMENT # 57

          0582  2A0B00        LHLD     TD
          0585  7C           MOV      A,H
          0586  4F           MOV      C,A
          0587  CD0000        CALL     NMOUT
58  2          CALL NMOUT(LOW(TD));
                                     ; STATEMENT # 58

          058A  2A0B00        LHLD     TD
          058D  7D           MOV      A,L
          058E  4F           MOV      C,A
          058F  CD0000        CALL     NMOUT

59  2          CALL CO(' ');
                                     ; STATEMENT # 59

          0592  0E20          MVI      C,20H
          0594  CD0000          CALL      CO
60  2          CALL CO(' ');
                                     ; STATEMENT # 60

          0597  0E20          MVI      C,20H
          0599  CD0000          CALL      CO
61  2          CALL CO('T');
                                     ; STATEMENT # 61

          059C  0F54          MVI      C,54H
          059E  CD0000          CALL      CO
62  2          CALL CO('H');
                                     ; STATEMENT # 62

          05A1  0E48          MVI      C,48H
          05A3  CD0000          CALL      CO
63  2          CALL CO('E');

```

```

; STATEMENT # 63
05A6 0E45 MVI C,45H
05A8 CD0000 CALL CO
64 2 CALL CO('T');
; STATEMENT # 64
05AB 0E54 MVI C,54H
05AD CD0000 CALL CO
65 2 CALL CO('A');
; STATEMENT # 65
05B0 0E41 MVI C,41H
05B2 CD0000 CALL CO
66 2 CALL CO('=');
; STATEMENT # 66
05B5 0E3D MVI C,3DH
05B7 CD0000 CALL CO
67 2 CALL NMOUT(LOW(THETA));
; STATEMENT # 67
05BA 2A0100 LHLD THETA
05BD 7D MOV A,L
05BE 4F MOV C,A
05BF CD0000 CALL NMOUT
68 2 CALL CC(0DH);
; STATEMENT # 68
05C2 0E0D MVI C,0DH
05C4 CD0000 CALL CO
69 2 CALL CO(0AH);
; STATEMENT # 69
05C7 0E0A MVI C,0AH
05C9 CD0000 CALL CO
70 2 END TMP;
; STATEMENT # 70
05CC C9 RET
71 1 FWD:PROCEDURE; /*PULSES THE MOTOR CONTROL THAT
; STATEMENT # 71
; PROC FWD
OPENS THE SOLAR DAMPER(1.8DEG/PULSE)*/
72 2 OE4=OE4 AND 0EFH; /*SET BIT 4--PORT E4
; STATEMENT # 72
HAS INVERTED OUTPUTS*/
05CD 3A0000 LDA OE4
05D0 E6EF ANI 0EFH
05D2 320000 STA OE4
73 2 OUTPUT(OE4H)=OE4;
; STATEMENT # 73
05D5 D3E4 OUT OE4H
74 2 DO I=1 TO 5;
; STATEMENT # 74
05D7 210F00 LXI H,I
05DA 3601 MVI M,1H
@20:
05DC 3F05 MVI A,5H
05DE 210F00 LXI H,I
05E1 BE CMP M
05E2 DAF105 JC @21
75 3 CALL TIME(100); /*10 MS DELAY*/

```

```

; STATEMENT # 75
05E5 3E64 MVI A,64H
05E7 CD0000 CALL GP0105
76 3 END;

; STATEMENT # 76
05EA 210F00 LXI H,I
05ED 34 INR M
05EF C2DC05 JNZ Q20

Q21:
77 2 OE4=OE4 OR 10H; /*ZERO BIT 4*/
; STATEMENT # 77
05F1 3A0000 LDA OE4
05F4 F610 ORI 10H
05F6 320000 STA OE4
78 2 OUTPUT(OE4H)=OE4;
; STATEMENT # 78
05F9 D3E4 OUT OE4H
79 2 DO I=1 TO 5;
; STATEMENT # 79
05FB 210F00 LXI H,I
05FE 3601 MVI M,1H
Q22:
0600 3E05 MVI A,5H
0602 210F00 LXI H,I
0605 BE CMP M
0606 DA1506 JC Q23
80 3 CALL TIME(100);
; STATEMENT # 80
0609 3E64 MVI A,64H
060B CD0000 CALL GP0105
81 3 END;
; STATEMENT # 81
060E 210F00 LXI H,I
0611 34 INR M
0612 C20006 JNZ Q22
Q23:
82 2 END FWD;
; STATEMENT # 82
0615 C9 RET
83 1 DELAY:PROCEDURE;
; STATEMENT # 83
; PROC DELAY
84 2 DO I=1 TO 4;
; STATEMENT # 84
0616 210F00 LXI H,I
0619 3601 MVI M,1H
Q24:
061B 3E04 MVI A,4H
061D 210F00 LXI H,I
0620 BE CMP M
0621 DA4506 JC Q25
85 3 DO J=1 TO 250; /*10 SEC DELAY*/
; STATEMENT # 85
0624 210E00 LXI H,J
0627 3601 MVI M,1H
Q26:

```

```

0629 3EFA MVI A,0FAH
062B 210E00 LXI H,J
062E BE CMP M
062F DA3E06 JC Q27
86 4 CALL TIME(100); ; STATEMENT # 86
0632 3E64 MVI A,64H
0634 CD0000 CALL GP0105
87 4 END; ; STATEMENT # 87
0637 210E00 LXI H,J
063A 34 INR M
063E C22906 JNZ Q26
88 3 Q27:
END; ; STATEMENT # 88
063E 210F00 LXI H,I
0641 34 INR M
0642 C21B06 JNZ Q24
89 2 Q25:
END DELAY; ; STATEMENT # 89
0645 C9 RET
/*THE FOLLOWING PROCEDURE OPENS SOLAR DAMPER TO MAX POSITION(90DEG)
90 1 DEG90:PROCEDURE; ; STATEMENT # 90
; PROC DEG90
91 2 DO WHILE(SHR(INPUT(0E6H),1)); ; STATEMENT # 91
Q28:
0646 DBE6 IN 0E6H
0648 B7 ORA A
0649 1F RAR
064A 1F RAR
064B D25406 JNC Q29
92 3 CALL FWD; ; STATEMENT # 92
064F CDCD05 CALL FWD
93 3 END; ; STATEMENT # 93
0651 C34606 JMP Q28
94 2 Q29:
THETA=50; ; STATEMENT # 94
0654 213200 LXI H,32H
0657 220100 SHLD THETA
95 2 END DEG90; ; STATEMENT # 95
065A C9 RET
96 1 BKWD:PROCEDURE; /*PULSES MOTOR CONTROL TO
; STATEMENT # 96
; PROC BKWD
CLOSE SOLAR DAMPER(1.8DEG/PULSE)*/

```



```

97      2      OE4=OE4 AND 0F7H;      /*SET BIT 3*/
                                           ; STATEMENT # 97
      065B 3A0000      LDA      OE4
      065E E6F7      ANI      0F7H
      0660 320000      STA      OE4
98      2      OUTPUT(0E4H)=OE4;      /*RAISE CONTROL LINE
                                           ; STATEMENT # 98
                                           FOR FWK(CW) PULSES*/
      0663 D3E4      OUT      0E4H
99      2      DO I=1 TO 5;
                                           ; STATEMENT # 99
      0665 210F00      LXI      H,I
      0668 3601      MVI      M,1H
      @30:
      066A 3E05      MVI      A,5H
      066C 210F00      LXI      H,I
      066F BE      CMP      M
      0670 DA7F06      JC      @31
100     3      CALL TIME(100);      /*10 MS DELAY*/
                                           ; STATEMENT # 100
      0673 3E64      MVI      A,64H
      0675 CD0000      CALL     @P0105
101     3      END;
                                           ; STATEMENT # 101
      0678 210F00      LXI      H,I
      067B 34      INR      M
      067C C2EA06      JNZ     @30
      @31:
102     2      OE4=OE4 OR 8H;      /*ZERO BIT 3*/
                                           ; STATEMENT # 102
      067F 3A0000      LDA      0F4
      0682 F608      ORI      8H
      0684 320000      STA      OE4
103     2      OUTPUT(0E4H)=0F4;      /*LOWER CONTROL LINE*/
                                           ; STATEMENT # 103
      0687 D3E4      OUT      0E4H
104     2      DO I=1 TO 5;
                                           ; STATEMENT # 104
      0689 210F00      LXI      H,I
      068C 3601      MVI      M,1H
      @32:
      068F 3E05      MVI      A,5H
      0690 210F00      LXI      H,I
      0693 BE      CMP      M
      0694 DAA306      JC      @33
105     3      CALL TIME(100);
                                           ; STATEMENT # 105
      0697 3E64      MVI      A,64H
      0699 CD0000      CALL     @P0105
106     3      END;
                                           ; STATEMENT # 106
      069C 210F00      LXI      H,I
      069F 34      INR      M
      06A0 C28E06      JNZ     @32
      @33:
107     2      END BKWD;
                                           ; STATEMENT # 107

```

36A3 C9

RET

```

108 1      INIT:OE4=0FFH;          /*INITIALIZE CONTROL WORD
                                ; STATEMENT # 108
00CC 310000      LXI      SP,@STACK$ORIGIN
                                INIT:
                                FOR PORT E4*/

00CF 210000      LXI      H,OE4
00D2 36FF        MVI      M,0FFH
109 1      OUTPUT(0EBH)=38H;      ; STATEMENT # 109

00D4 3F98        MVI      A,98H
00D6 D3EB        OUT      0FBH
110 1      OUTPUT(0E7H)=89H;      ; STATEMENT # 110

00D8 3E89        MVI      A,89H
00DA D3E7        OUT      0E7H
111 1      START:DO WHILE (INPUT(0EEH)); /*CLOSE DAMPER TO SOLAR AIR*/
                                ; STATEMENT # 111
                                START:
                                Q34:
00DC DBE6        IN        0EEH
00DE 1F          RAR
00DF D2E820      JNC      Q35
112 2      CALL BKWD;            ; STATEMENT # 112
00E2 CD5B06      CALL      BKWD
113 2      END;                  ; STATEMENT # 113
00E5 C3DC00      JMP      Q34
114 1      Q35:
                                THETA=0;
                                ; STATEMENT # 114

00E8 210000      LXI      H,0H
00EB 220100      SHLD     THETA
115 1      SOLAR:LPN=1;          ; STATEMENT # 115
                                SOLAR:
00EF 210100      LXI      H,1H
00F1 220500      SHLD     LPN
116 1      CALL CO(0AH);         ; STATEMENT # 116
00F4 0E0A        MVI      C,0AH
00F6 CD0000      CALL      CO
117 1      CALL CO(0DH);         ; STATEMENT # 117
00F9 0FED        MVI      C,0DH
00FB CD0000      CALL      CO
118 1      CALL CO('S');         ; STATEMENT # 118
00FE 0E53        MVI      C,53H
0100 CD0000      CALL      CO
119 1      CALL CO('O');

```

; STATEMENT # 119

```

120 1 0103 0E4F MVI C,4FH
      0105 CD0000 CALL CO
      CALL CO('I');
; STATEMENT # 120
121 1 0108 0E4C MVI C,4CH
      010A CD0000 CALL CO
      CALL CO('A');
; STATEMENT # 121
122 1 010D 0E41 MVI C,41H
      010F CD0000 CALL CO
      CALL CO('R');
; STATEMENT # 122
123 1 0112 0E52 MVI C,52H
      0114 CD0000 CALL CO
      CALL CO(0DH);
; STATEMENT # 123
124 1 0117 0E0E MVI C,0EH
      0119 CD0000 CALL CO
      CALL CO(0AH);
; STATEMENT # 124
125 1 011C 0E0A MVI C,0AH
      011E CD0000 CALL CO
      CALL TMP;
; STATEMENT # 125
126 1 0121 CD7904 CALL TMP
      IF(TS>U)THEN GOTO MIX;
; STATEMENT # 126
      0124 110200 LXI D,U
      0127 010700 LXI E,TS
      012A CD0000 CALL 0F0098
      012D D23301 JNC 01
; STATEMENT # 127
      0130 C30702 JMP MIX
      01:
128 1 CALL DEG90; /*TS<U,SOLAR AIR MAX*/
; STATEMENT # 128
129 1 0133 CD4606 CALL DEG90
      IF(TS<L)THEN GOTO BURNER;
; STATEMENT # 129
      0136 010000 LXI B,L
      0139 110700 LXI D,TS
      013C CD0000 CALL 0F0098
      013F D24501 JNC 02
; STATEMENT # 130
      0142 C34B01 JMP BURNER
      02:
131 1 ELSE CALL DELAY; /*ELSE L<TS<U;SO STAY
; STATEMENT # 131
      0145 CD1606 CALL DELAY
      03:
; STATEMENT # 132
132 1 GOTO SOLAR;
; STATEMENT # 132
      0148 C3FE00 JMP SOLAR
133 1 BURNER: LPN=2;

```

; STATEMENT # 133

BURNER:

```

014B 210200 LXI H,2H
014E 220500 SHLD LPN
134 1 CUTPUT(0E4H)=(0E4 AND 0DFH); /*LIGHT BURNER*/
; STATEMENT # 134

```

```

0151 3A0000 LDA 0E4
0154 E61F ANI 0DFH
0156 D3E4 OUT 0E4H
135 1 INTCON: CALL CO('B');

```

; STATEMENT # 135

INTCON:

```

0158 0E42 MVI C,42H
015A CD0000 CALL CO
136 1 CALL CO('U');

```

; STATEMENT # 136

```

015D 0E55 MVI C,55H
015F CD0000 CALL CO
137 1 CALL CO('R');

```

; STATEMENT # 137

```

0162 0E52 MVI C,52H
0164 CD0000 CALL CO
138 1 CALL CO('N');

```

; STATEMENT # 138

```

0167 0E4E MVI C,4EH
0169 CD0000 CALL CO
139 1 CALL CO('E');

```

; STATEMENT # 139

```

016C 0E45 MVI C,45H
016E CD0000 CALL CO
140 1 CALL CO('R');

```

; STATEMENT # 140

```

0171 0E52 MVI C,52H
0173 CD0000 CALL CO
141 1 CALL CO(0DH);

```

; STATEMENT # 141

```

0176 0E0D MVI C,0DH
0178 CD0000 CALL CO
142 1 CALL CO(0AH);

```

; STATEMENT # 142

```

017B 0E0A MVI C,0AH
017D CD0000 CALL CO
143 1 CALL TMP;

```

; STATEMENT # 143

```

0180 CD7904 CALL TMP
144 1 IF (TD<L+(U-L)/2) THEN CALL DELAY;
; STATEMENT # 144

```

```

0183 010000 LXI B,L
0186 110200 LXI I,U
0189 CD0000 CALL 0F0098
018C EB XCHG
018D 210200 LXI H,2H
0190 CD0000 CALL 0F0029
0193 2A0000 LHLD L
0196 19 DAD D
0197 110B00 LXI D,TD

```

```

019A CD0000 CALL QP0102
019D D2A601 JNC Q4 ; STATEMENT # 145

01A0 CD1606 CALL DELAY
01A3 C3A901 JMP Q5

146 1 Q4:
ELSE GO TO BRNOFF; ; STATEMENT # 146

01A6 C3AC01 JMP BRNCFB

147 1 Q5:
GO TO INTCON; ; STATEMENT # 147

01A9 C35801 JMP INTCON
148 1 BRNCFB: 0E4=0E4 OR 20H; /*ZERO BIT 5 OF PORT1*/
; STATEMENT # 148

BRNOFF:
01AC 3A0000 LDA 0E4
01AF F620 ORI 20H
01B1 320000 STA 0E4
149 1 OUTPUT(0E4H)=0E4; /*TURN OFF BURNER*/
; STATEMENT # 149

01B4 D3F4 OUT 0E4H
150 1 LCOP:LPN=3; ; STATEMENT # 150

LOOP:
01B6 210300 LXI H,3H
01B9 220500 SHLD IPN
151 1 CALL CO('I'); ; STATEMENT # 151

01BC 0E4C MVI C,4CH
01BE CD0000 CALL CO
152 1 CALL CO('O'); ; STATEMENT # 152

01C1 0E4F MVI C,4FH
01C3 CD0000 CALL CO
153 1 CALL CO('O'); ; STATEMENT # 153

01C6 0E4F MVI C,4FH
01C8 CD0000 CALL CO
154 1 CALL CO('P'); ; STATEMENT # 154

01CB 0E50 MVI C,50H
01CD CD0000 CALL CO
155 1 CALL CO(0AH); ; STATEMENT # 155

01D0 0E2A MVI C,0AH
01D2 CD0000 CALL CO
156 1 CALL CO(0DH); ; STATEMENT # 156

01D5 0E0E MVI C,0EH
01D7 CD0000 CALL CO
157 1 CALL TMP; ; STATEMENT # 157

01DA CD7904 CALL TMP
158 1 IF (TS<1)THEN CALL DELAY;

```

```

                                ; STATEMENT # 158
01DE 010000      LXI      B,L
01E0 110720      LXI      D,TS
01E3 CD0000      CALL     @P0098
01E6 D2EF01      JNC      @6
                                ; STATEMENT # 159
01E9 CD1606      CALL     DELAY
01EC C3F231      JMP      @7
160 1          @6:      ELSE GOTO SOLAR;
                                ; STATEMENT # 160
01EF C3FE00      JMP      SOLAR
161 1          @7:      CALL TMP;
                                ; STATEMENT # 161
01F2 CD7904      CALL     TMP
162 1          IF(TD<L)THEN GOTO BURNER; /*IF TD<L & TS<I*/
                                ; STATEMENT # 162
01F5 010000      LXI      B,L
01F8 110B00      LXI      D,TD
01FB CD0000      CALL     @P0098
01FE D20402      JNC      @8
                                ; STATEMENT # 163
0201 C34B01      JMP      BURNER
164 1          @8:      ELSE GOTO LOOP; /*IF TD>L & TS<I*/
                                ; STATEMENT # 164
0204 C3B601      JMP      LOOP
165 1          @9:
MIX:LPN=4;
                                ; STATEMENT # 165
MIX:
0207 210400      LXI      H,4H
020A 220500      SHLD     LPN
166 1          CALL CO('M');
                                ; STATEMENT # 166
020D 0E4D        MVI      C,4DH
020F CD0000      CALL     CO
167 1          CALL CO('I');
                                ; STATEMENT # 167
0212 0E49        MVI      C,49H
0214 CD0000      CALL     CO
168 1          CALL CO('X');
                                ; STATEMENT # 168
0217 0E58        MVI      C,58H
0219 CD0000      CALL     CO
169 1          CALL CO(0AH);
                                ; STATEMENT # 169
021C 0E0A        MVI      C,0AH
021F CD0000      CALL     CO
170 1          CALL CO(0DH);
                                ; STATEMENT # 170
0221 0E0D        MVI      C,0DH
0223 CD0000      CALL     CO
171 1          CALL TMP;

```

; STATEMENT # 171

/*CHECK DAMPER POSITION; IF FULLY OPEN, THETA=50*/

```

172  1  0226  CD7904          CALL    TMP
          IF((INPUT(0E6H) AND 1)=0)THEN THETA=0;
                                     ; STATEMENT # 172

```

```

          0229  DBE6          IN      0E6H
          022F  E601          ANI     1H
          022B  FE00          CPI     0H
          022F  C23802        JNZ     010
                                     ; STATEMENT # 173

```

```

          0232  210000        LXI     H,0H
          0235  220100        SHLD    THETA

```

```

          010:
174  1          IF((INPUT(0E6H) AND 2)=0)THEN THETA=50;
                                     ; STATEMENT # 174

```

```

          0238  DBE6          IN      0E6H
          023A  E602          ANI     2H
          023C  FE00          CPI     0H
          023E  C24702        JNZ     011
                                     ; STATEMENT # 175

```

/*ITERATIVE PROCEDURE FOR DETERMINING
THEORETICAL SETTING ,GIVEN TS & TA*/

```

          0241  213200        LXI     H,32H
          0244  220100        SHLD    THETA

```

011:

```

176  1          N,A=32;
                                     ; STATEMENT # 176

```

```

          0247  212000        LXI     H,20H
          024A  220300        SHLD    N
          024D  7D           MOV     A,L
          024F  321000        STA     A

```

```

177  1          CALL CO('I');
                                     ; STATEMENT # 177

```

```

          0251  0E49          MVI     C,49H
          0253  CD0000        CALL    CO

```

```

178  1          CALL CO('T');
                                     ; STATEMENT # 178

```

```

          0256  0E54          MVI     C,54H
          0258  CD0000        CALL    CO

```

```

179  1          CALL CO('E');
                                     ; STATEMENT # 179

```

```

          025B  0E45          MVI     C,45H
          025D  CD0000        CALL    CO

```

```

180  1          CALL CO('R');
                                     ; STATEMENT # 180

```

```

          0260  0E52          MVI     C,52H
          0262  CD0000        CALL    CO

```

```

181  1          CALL CO(0DH);
                                     ; STATEMENT # 181

```

```

          0265  0E0D          MVI     C,0DH
          0267  CD0000        CALL    CO

```

```

182  1          CALL CO(0AH);
                                     ; STATEMENT # 182

```

```

026A 0E0A      MVI      C,0AH
026C CD0000      CALL     CO
183   1      ITER:   DO I=0 TO 5;
                                ; STATEMENT # 183
                                ITER:
026F 210F00      LXI      H,I
0272 3600      MVI      M,0H
                                Q36:
0274 3E05      MVI      A,5H
0276 210F00      LXI      H,I
0279 BE          CMP      M
027A DA2103      JC       Q37
184   2      TD=(TS*10/KS(N)+TA*10/KA(N))*10;
                                ; STATEMENT # 184
027D 210700      LXI      H,TS
0280 CD0000      CALL     QP0031
0283 F5          PUSH     H          ; 1
0284 2A0300      LHLD     N
0287 010400      LXI      P,KS
028A 29          DAD      H
028B 09          DAD      B
028C 4F          MOV      C,M
028D 23          INX      H
028E 46          MOV      E,M
028F D1          POP      D          ; 1
0290 CD0000      CALL     QP0030
0293 210900      LXI      H,TA
0296 D5          PUSH     D          ; 1
0297 CD0000      CALL     QP0031
029A E5          PUSH     H          ; 2
029B 2A0300      LHLD     N
029E 016800      LXI      E,KA
02A1 29          DAD      H
02A2 09          DAD      B
02A3 4F          MOV      C,M
02A4 23          INX      H
02A5 46          MOV      E,M
02A6 D1          POP      D          ; 2
02A7 CD0000      CALL     QP0030
02AA E1          POP      H          ; 1
02AB 19          DAD      D
02AC CD0000      CALL     QP0033
02AF 220B00      SHLD     TD
185   2      A=SHR(A,1);
                                ; STATEMENT # 185
02B2 3A1000      LDA      A
02B5 B7          ORA      A
02B6 1F          RAR
02B7 321000      STA      A
186   2      IF(TD>U)THEN N=N-SHL(A,1)+A;
                                ; STATEMENT # 186
02BA 110200      LXI      D,U
02BD CD0000      CALL     QP0102
02C0 D21A02      JNC      Q12
                                ; STATEMENT # 187
02C3 3A1000      LDA      A
02C6 87          ADD      A

```


		02C7	110300	LXI	D,N	
		02CA	CD0000	CALL	GP0101	
		02CD	E5	PUSH	H	; 1
		02CE	2A1000	LHLD	A	
		02D1	2600	MVI	H,0	
		02D3	C1	POP	E	; 1
		02D4	09	DAD	E	
		02D5	EF	XCHG		
		02D6	2B	DCX	H	
		02D7	73	MOV	M,E	
		02D8	23	INX	H	
		02D9	72	MOV	M,D	
				@12:		
188	2			IF(TD<L)THEN N=N+A;		; STATEMENT # 188
		02DA	010000	LXI	P,L	
		02DD	110B00	LXI	D,TD	
		02E0	CD0000	CALL	GP0098	
		02E3	D2F402	JNC	@13	; STATEMENT # 189
		02E6	3A1000	LDA	A	
		02E9	110300	LXI	D,N	
		02EC	CD0000	CALL	GP0014	
		02EF	EB	XCHG		
		02F0	2B	DCX	H	
		02F1	73	MOV	M,E	
		02F2	23	INX	H	
		02F3	72	MOV	M,D	
				@13:		
190	2			CALL CO(' ');		; STATEMENT # 190
		02F4	0E20	MVI	C,20H	
		02F6	CD0000	CALL	CO	
191	2			CALL CO('N');		; STATEMENT # 191
		02F9	0E4E	MVI	C,4EH	
		02FB	CD0000	CALL	CO	
192	2			CALL CO('=');		; STATEMENT # 192
		02FE	0E3D	MVI	C,3DH	
		0300	CD0000	CALL	CO	
193	2			CALL NMOUT(LOW(N));		; STATEMENT # 193
		0303	2A0300	LHLD	N	
		0306	7D	MOV	A,L	
		0307	4F	MOV	C,A	
		0308	CD0000	CALL	NMOUT	
194	2			CALL CO(0DH);		; STATEMENT # 194
		030B	0F0D	MVI	C,0DH	
		030D	CD0000	CALL	CO	
195	2			CALL CO(0AH);		; STATEMENT # 195
		0310	0E0A	MVI	C,0AH	
		0312	CD0000	CALL	CO	
196	2			IF(N>49)THEN N=48;		; STATEMENT # 196

		0315 3E31	MVI	A,31H	
		0317 210300	LXI	H,N	
		031A CD0000	CALL	QP0103	
		031D D22603	JNC	Q14	
					; STATEMENT # 197
		0320 213000	LXI	H,30H	
		0323 220300	SHLD	N	
198	2				
					; STATEMENT # 198
		0326 210F00	LXI	H,I	
		0329 34	INR	M	
		032A C27402	JNZ	Q36	
199	1				
				DO WHILE (N<THETA);	
					; STATEMENT # 199
		032D 010100	LXI	B,THETA	
		0330 110300	LXI	D,N	
		0333 CD0000	CALL	QP0098	
		0336 D24603	JNC	Q39	
200	2			CALL BKWD;	
					; STATEMENT # 200
		0339 CD5B06	CALL	BKWD	
201	2			THETA=THETA-1;	
					; STATEMENT # 201
		033C 2A0100	LHLD	THETA	
		033F 2B	DCX	H	
		0340 220100	SHLD	THETA	
202	2			END;	
					; STATEMENT # 202
		0343 C32D03	JMP	Q38	
203	1			DO WHILE(N>THETA);	
					; STATEMENT # 203
		0346 110100	LXI	D,THETA	
		0349 010300	LXI	E,N	
		034C CD0000	CALL	QP0098	
		034F D25F03	JNC	Q41	
204	2			CALL FWD;	
					; STATEMENT # 204
		0352 CDCD05	CALL	FWD	
205	2			THETA=THETA+1;	
					; STATEMENT # 205
		0355 2A0100	LHLD	THETA	
		0358 23	INX	H	
		0359 220100	SHLD	THETA	
206	2			END;	
					; STATEMENT # 206
		035C C34603	JMP	Q40	
207	1			CALL CO('T');	
					; STATEMENT # 207
		035F 0E54	MVI	C,54H	
		0361 CD0000	CALL	CO	

```

208 1          CALL CO('H');
                                ; STATEMENT # 208
      0364 0E48      MVI      C,4EH
      0366 CD0000      CALL      CO
209 1          CALL CO('E');
                                ; STATEMENT # 209
      0369 0E45      MVI      C,45H
      036B CD0000      CALL      CO
210 1          CALL CO('T');
                                ; STATEMENT # 210
      036E 0E54      MVI      C,54H
      0370 CD0000      CALL      CO
211 1          CALL CO('A');
                                ; STATEMENT # 211
      0373 0E41      MVI      C,41H
      0375 CD0000      CALL      CO
212 1          CALL CO('=');
                                ; STATEMENT # 212
      0378 0E3D      MVI      C,3DH
      037A CD0000      CALL      CO
213 1          CALL NMOUT(LOW(THETA));
                                ; STATEMENT # 213
      037E 2A0100      LHLD      THETA
      0380 7D          MOV      A,L
      0381 4F          MOV      C,A
      0382 CD0000      CALL      NMOUT
214 1          CALL CO(0DH);
                                ; STATEMENT # 214
      0385 0E0D      MVI      C,0DH
      0387 CD0000      CALL      CO
215 1          CALL CO(0AH);
                                ; STATEMENT # 215
      038A 0E0A      MVI      C,0AH
      038C CD0000      CALL      CO

      /*THIS ROUTINE WILL MAINTAIN THE CORRECT DAMPER SETTING
        FOR THE DESIRED DRYER TEMPERATURE*/

216 1          MAINT: 0E4=(0E4 AND 0F8H) OR 6;
                                ; STATEMENT # 216
      MAINT:
      038E 3A0000      LDA      0E4
      0392 E6F8      ANI      0F8H
      0394 F606      ORI      6H
      0396 320000      STA      0E4
217 1          OUTPUT(0E4H)=0E4;
                                /*SELECT TD*/
                                ; STATEMENT # 217
      0399 D3E4      OUT      0E4H
218 1          OUTPUT(0EAH)=1;
                                ; STATEMENT # 218
      039B 3E01      MVI      A,1H
      039D D3EA      OUT      0EAH
219 1          OUTPUT(0EAH)=0;
                                ; STATEMENT # 219
      039F 3E00      MVI      A,0H
      03A1 D3EA      OUT      0EAH
220 1          CALL CO('M');

```

```

; STATEMENT # 220
221 1 03A3 0E4D MVI C,4DH
03A5 CD0000 CALL CO
CALL CO('A');
; STATEMENT # 221
222 1 03A8 0E41 MVI C,41H
03AA CD0000 CALL CO
CALL CO('I');
; STATEMENT # 222
223 1 03AD 0E49 MVI C,49H
03AF CD0000 CALL CO
CALL CO('N');
; STATEMENT # 223
224 1 03B2 0E4F MVI C,4FH
03B4 CD0000 CALL CO
CALL CO('T');
; STATEMENT # 224
225 1 03B7 0E54 MVI C,54H
03B9 CD0000 CALL CO
CALL CO(0AH);
; STATEMENT # 225
226 1 03BC 0E0A MVI C,0AH
03BE CD0000 CALL CO
CALL CO(0DH);
; STATEMENT # 226
227 1 03C1 0E0D MVI C,0DH
03C3 CD0000 CALL CO
CALL DELAY; /*10 SEC DELAY*/
; STATEMENT # 227
228 1 03C6 CD1606 CALL DELAY
CALL TMP;
; STATEMENT # 228

```

/*THE FOLLOWING ROUTINES COMPENSATE FOR ANY POSSIBLE INACCURACIES
IN THE THEORETICAL CALCULATION FOR THE DAMPER SETTING*/

```

229 1 03C9 CD7924 CALL TMP
DCR: IF((TD>U) AND (THETA>0)) THEN DO;
; STATEMENT # 229
DCR:
03CC 110200 LXI D,U
03CF 010700 LXI E,TD
03D2 CD0000 CALL GP0098
03D5 9F SBB A
03D6 F5 PUSH PSW ; 1
03D7 3E00 MVI A,0H
03D9 210100 LXI H,THETA
03DC CD0000 CALL GP0103
03DF 9F SBB A
03E0 C1 POP B ; 1
03E1 48 MOV C,B
03E2 A1 ANA C
03E3 1F RAR
03E4 D2F103 JNC G15
231 2 THETA=THETA-1;
; STATEMENT # 231

```

```

      03E7 2A0100      LHLD  THETA
      03EA 2B          DCX   H
      03EB 220100      SHLD  THETA
232    2              CALL FWD;
                                ; STATEMENT # 232
      03EE CDCD05      CALL  FWD
233    2              END;
                                ; STATEMENT # 233
      015:
234    1      INCR:    IF((TD<L) AND (THETA<50)) THEN DO;
                                ; STATEMENT # 234
      INCR:
      03F1 010000      LXI    B,L
      03F4 110B00      LXI    D,TD
      03F7 CD0000      CALL   QP0098
      03FA 9F          SBB    A
      03FB F5          PUSH   PSW      ; 1
      03FC 3E32        MVI    A,32H
      03FE 110100      LXI    D,THETA
      0401 CD0000      CALL   QF0101
      0404 9F          SBB    A
      0405 C1          POP     B      ; 1
      0406 48          MOV    C,B
      0407 A1          ANA    C
      0408 1F          RAR
      0409 D21604      JNC    Q16
236    2              CALL FWD;
                                ; STATEMENT # 236
      040C CDCD05      CALL  FWD
237    2              THETA=THETA+1;
                                ; STATEMENT # 237
      040F 2A0100      LHLD  THETA
      0412 23          INX    H
      0413 220100      SHLD  THETA
238    2              END;
                                ; STATEMENT # 238
      Q16:
239    1      CALL TMP;
                                ; STATEMENT # 239

```

```

/*THIS ROUTINE WILL MAINTAIN DESIRED DRYER TEMP INDEFINITELY
UNLESS SOLAR TEMP DROPS BELOW LOWER LIMIT;
IN WHICH CASE, PROGRAM RETURNS TO SOLAR ROUTINE*/

```

```

240    1      0416 CD7904      CALL  TMP
              IF(TS<=1)THEN GOTO SOLAR;
                                ; STATEMENT # 240
      0419 110000      LXI    D,L
      041C 010700      LXI    B,TS
      041F CD0000      CALL   QF0098
      0422 DA2804      JC     Q17
                                ; STATEMENT # 241
      0425 C3FE00      JMP    SOLAR

```

```

/*IF THE DRYER COMPARTMENT BECCMES TOO HOT OR TC COOL,
AND THE DAMPER IS AT MIN OR MAX SETTING RESPECTIVELY,
AN ALARM LIGHT WILL BE ACTIVATED AND THE PROGRAM HALTED*/

```

Q17:

```

242      1      IF((TD>U) AND (THETA=0))THEN GO TO ALARM;
                                           ; STATEMENT # 242
0428      110200      LXI      D,U
042B      010B00      LXI      B,TD
042E      CD0000      CALL     GP0098
0431      9F          SBB      A
0432      F5          PUSH     PSW      ; 1
0433      3E00      MVI      A,0H
0435      110100      LXI      D,THETA
0438      CD0000      CALL     GP0101
043B      B5          ORA      L
043C      D601      SUI      1
043E      9F          SBB      A
043F      C1          POP      B      ; 1
0440      48          MOV      C,B
0441      A1          ANA      C
0442      1F          RAR
0443      D24924      JNC      Q18
                                           ; STATEMENT # 243
0446      C36D04      JMP      ALARM

```

Q18:

```

244      1      IF((TD<L) AND (THETA=50))THEN GOTO ALARM;
                                           ; STATEMENT # 244
0449      010000      LXI      P,L
044C      110B00      LXI      D,TD
044F      CD0000      CALL     GP0098
0452      9F          SBB      A
0453      F5          PUSH     PSW      ; 1
0454      3E32      MVI      A,32H
0456      110100      LXI      D,THETA
0459      CD0000      CALL     GP0101
045C      B5          ORA      L
045E      D601      SUI      1
045F      9F          SBB      A
0460      C1          POP      B      ; 1
0461      48          MOV      C,B
0462      A1          ANA      C
0463      1F          RAR
0464      D26A24      JNC      Q19
                                           ; STATEMENT # 245
0467      C36D04      JMP      ALARM

```

Q19:

```

246      1      GO TO MAINT;
                                           ; STATEMENT # 246
046A      C38F03      JMP      MAINT

247      1      ALARM:  OE4=OE4 AND 0BFH;  /*SET ALARM BIT*/
                                           ; STATEMENT # 247
                        ALARM:
046D      3A0000      LDA      OE4
0470      E6BF      ANI      0BFH
0472      320000      STA      OE4

248      1      OUTPUT(0E4H)=OE4;  /*RAISE ALARM LINE*/
                                           ; STATEMENT # 248

```

PL/M-80 COMPILER

```
      0475 D3E4          OUT      2E4H
249   1      END USDA;
      0477 FB
      0478 76          EI
                        HLT
                        ; STATEMENT # 249
```

MODULE INFORMATION:

```
CODE AREA SIZE      = 06A4H    1700D
VARIABLE AREA SIZE  = 0011H    17D
MAXIMUM STACK SIZE  = 0006H    6D
312 LINES READ
0 PROGRAM ERROR(S)
```

END OF PL/M-80 COMPIATION

APPENDIX C

REFERENCES

REFERENCES

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